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Cavity Beam Position Monitor for the ILC Main Linac: Status and Plans

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EAJADE
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Development Exchange Programme

Development of a **re-entrant cBPM for the ILC Main Linac**

Project in collaboration with KEK and CIEMAT: development of the cryostat for a BPM and a super-conducting quadrupole

Mechanical requirements:

Mechanical fit of the BPM and the SC quadrupole magnet
Cryogenic and UV conditions have to be met

Measurement requirements:

Spatial resolution $< 1 \mu\text{m}$

Temporal resolution $< 369 \text{ ns}$

The designed BPM will initially be tested at ATF at warm and cryogenic conditions after installation of the test cryomodule.

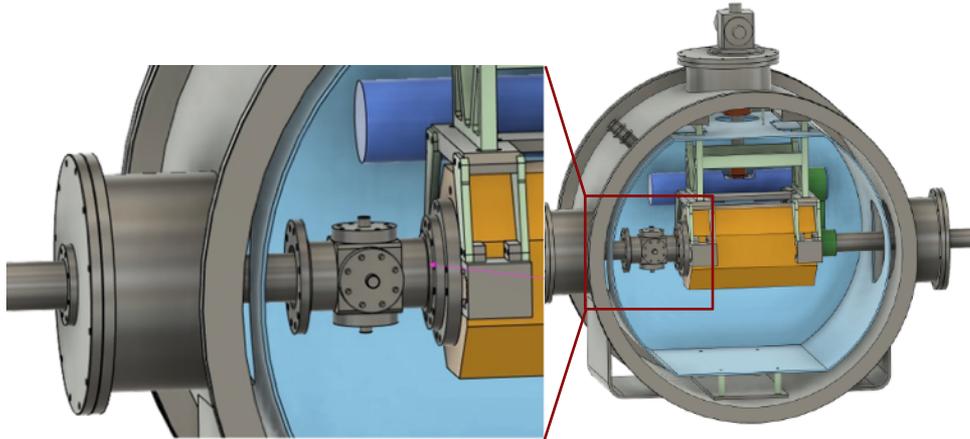


Figure: Cryostat accommodating BPM and SC quadrupole

Beam parameters	ATF	ILC
Bunch charge (nC)	1,6	3,2
Bunch spacing (ns)	150	369

Table: Relevant ATF and ILC parameters

I. Resonant cavity Beam Position Monitor

A) Pillbox cavity BPM

→ Working principle

Cavity BPMs are resonant systems crossed by the beam pipe. EM modes are induced on the cavity by the beam and their amplitude depends on the beam position.

Two modes in particular are of interest:

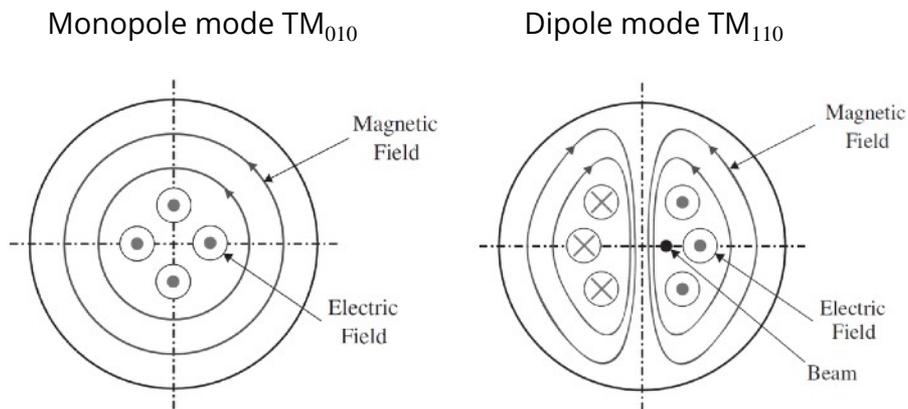


Figure: Cross-sectional view of the TM modes in a pillbox cavity

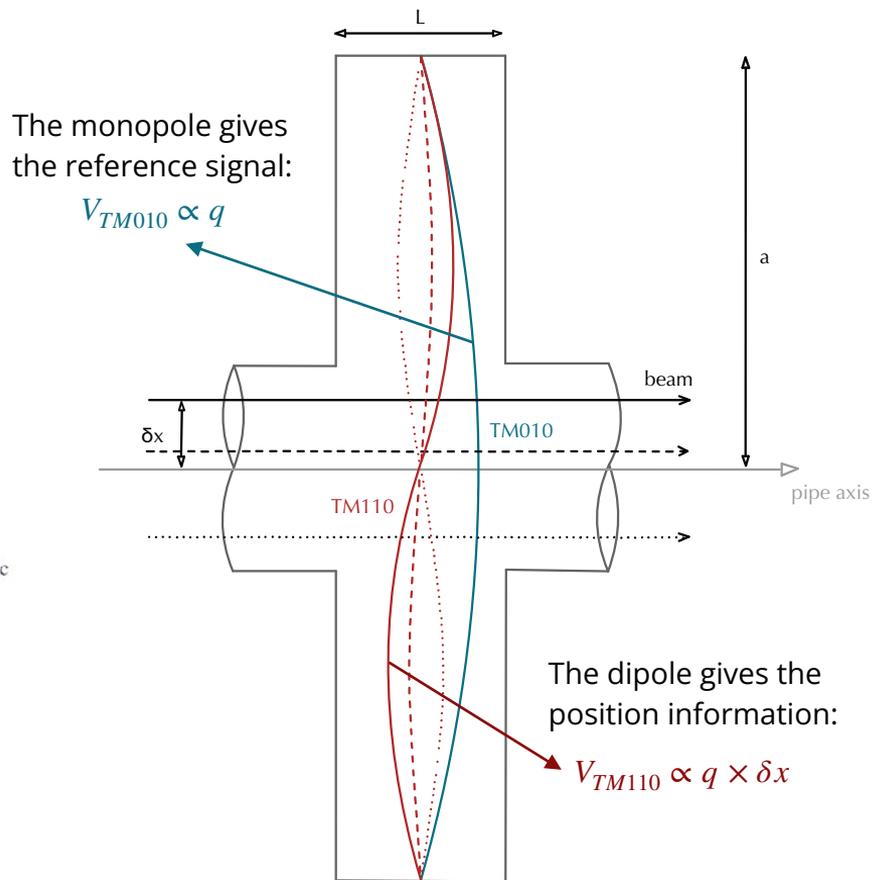
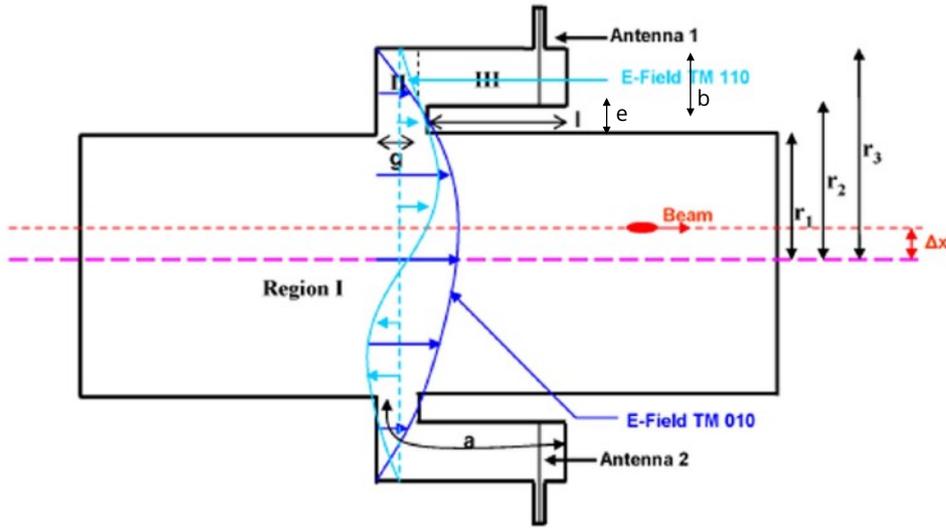


Figure: Representation of the E-fields induced in the cavity

I. Resonant cavity Beam Position Monitor

B) Re-entrant cavity BPM: a model from C. Simon - Saclay

The re-entrant cavity BPM



- I. Beam pipe
- II. Gap
- III. Coaxial cylinder

Figure: Scheme of the re-entrant cBPM

Saclay: Simon - Re-entrant cavity BPM for X-FEL

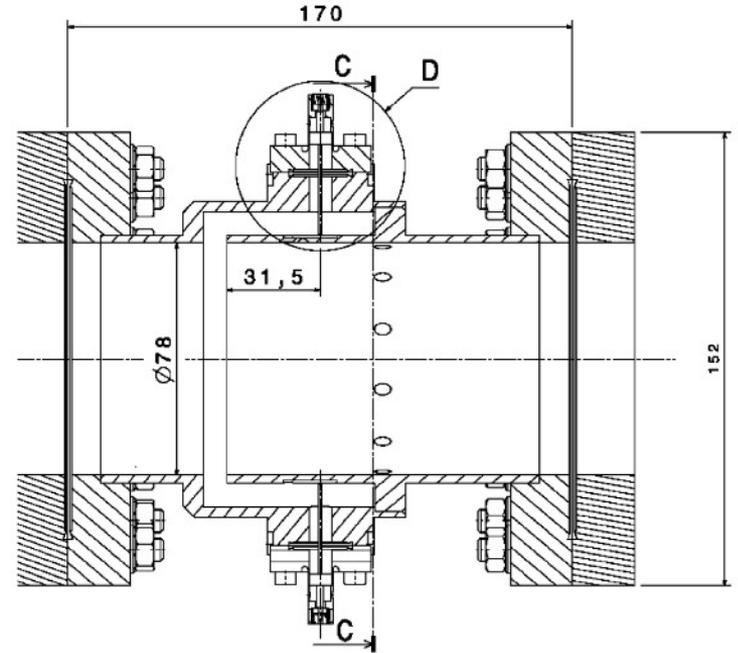
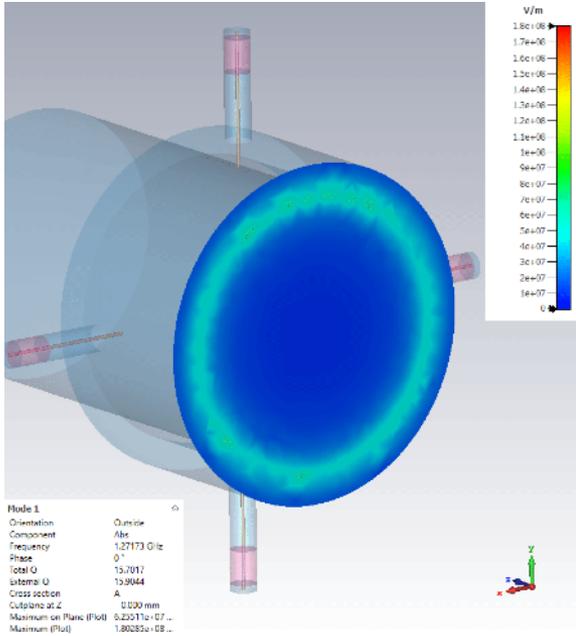


Figure: Design plans of cBPM from Saclay

I. Resonant Cavity BPM

Monopole mode TM_{010}

$$f_{010} = 1.25 \text{ GHz}$$



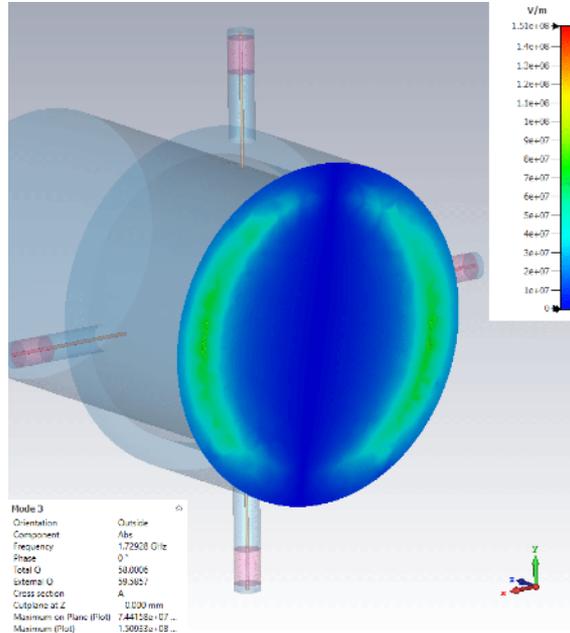
Yields reference signal

B) Re-entrant cavity BPM: a model from C. Simon - Saclay

Dipole mode TM_{110}

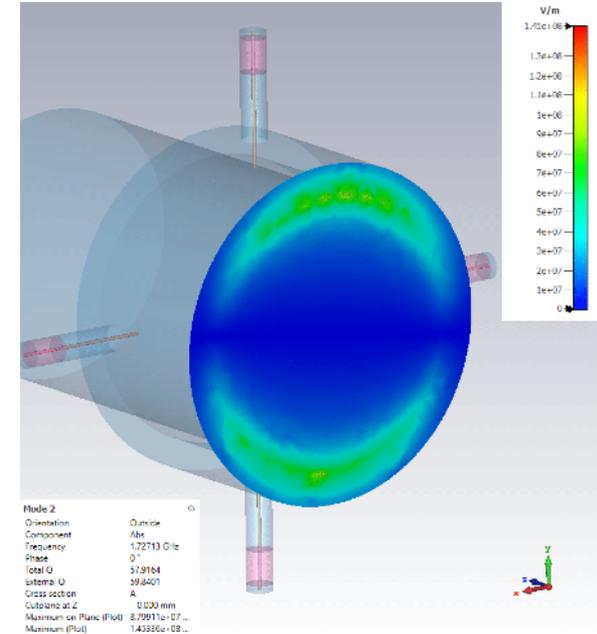
$$f_{010} = 1.72 \text{ GHz}$$

degeneration on x



Yields position signal on x

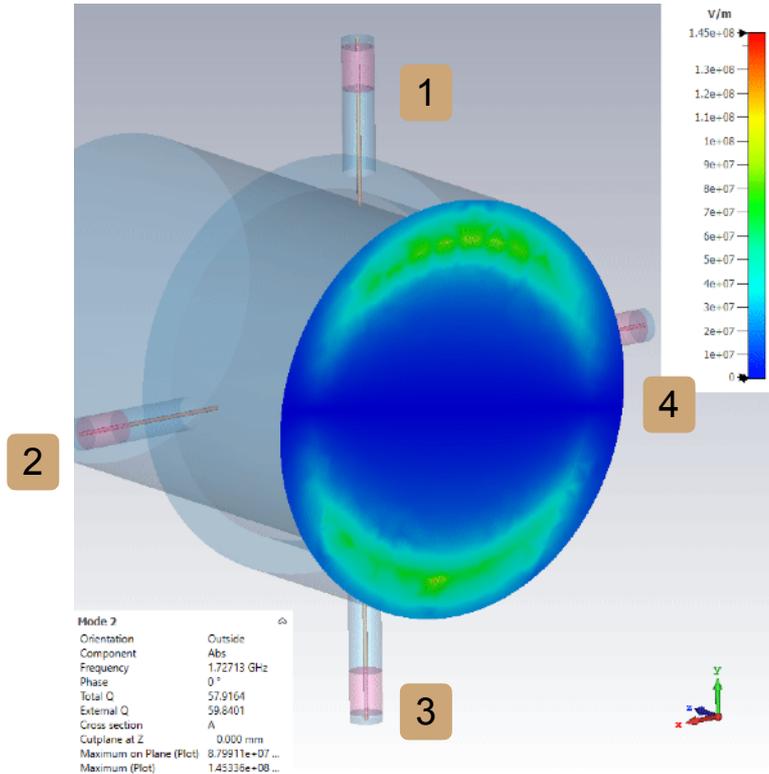
degeneration on y



Yields position signal on y

I. Resonant cavity Beam Position Monitor

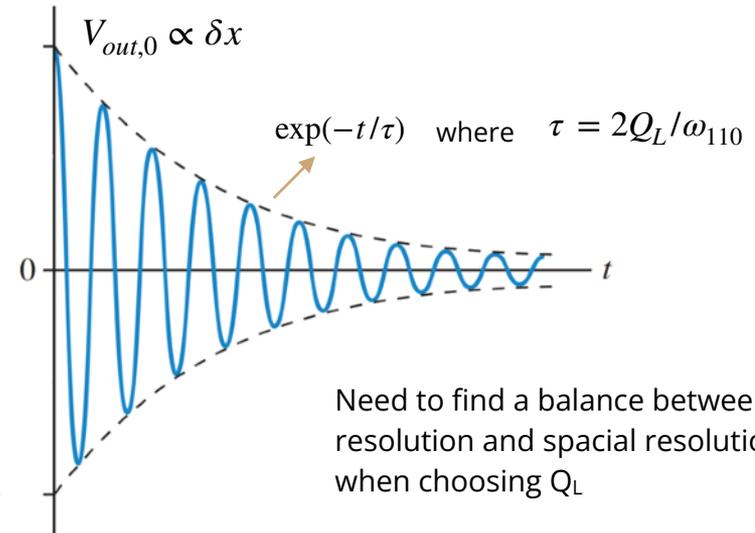
C) Signal extraction



→ **Output signal on the time domain:**

The position signal oscillates at the dipole mode resonance frequency and decays exponentially with decay constant τ :

$$V_{position}(t) = V_{out,0} \sin(\omega_{110}t + \varphi) \exp(-t/\tau)$$



Need to find a balance between time resolution and spatial resolution when choosing Q_L

II. Project definition and objectives

- ➔ **Modify an existing cBPM design to fit ILC demands and improve spacial resolution**

Challenges to overcome:

- ❖ Improve spacial resolution of the re-entrant cBPM (under 1 μm)
 - Modification of the cBPM design to improve:
 - sensitivity of the modes
 - loaded quality factor
 - Design of a read-out system that allows high resolution measurements
- ❖ Mechanical attachment and alignment with SC quadrupole
- ❖ cBPM and read-out system has to be suitable to perform measurements at ATF

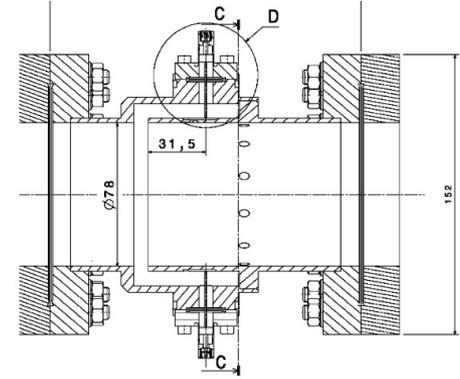


Figure: Design plans of cBPM from Saclay

	F (GHz)	Q	R/Q @10 mm
Monopole mode	1.25	24	13 Ω
Dipole mode	1.72	51.4	1.11 Ω
Resolution: around 4 μm			

III. Design studies of the cBPM

A) Geometry studies of the cBPM

- **Eigenmode solver in CST**

Evaluate the E and M fields distributions, coupling to antennas and the influence of geometrical parameters on the resonant frequency and quality factor Q_L

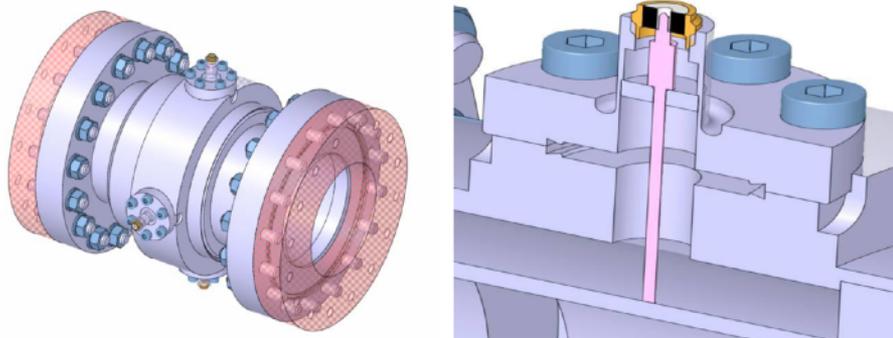
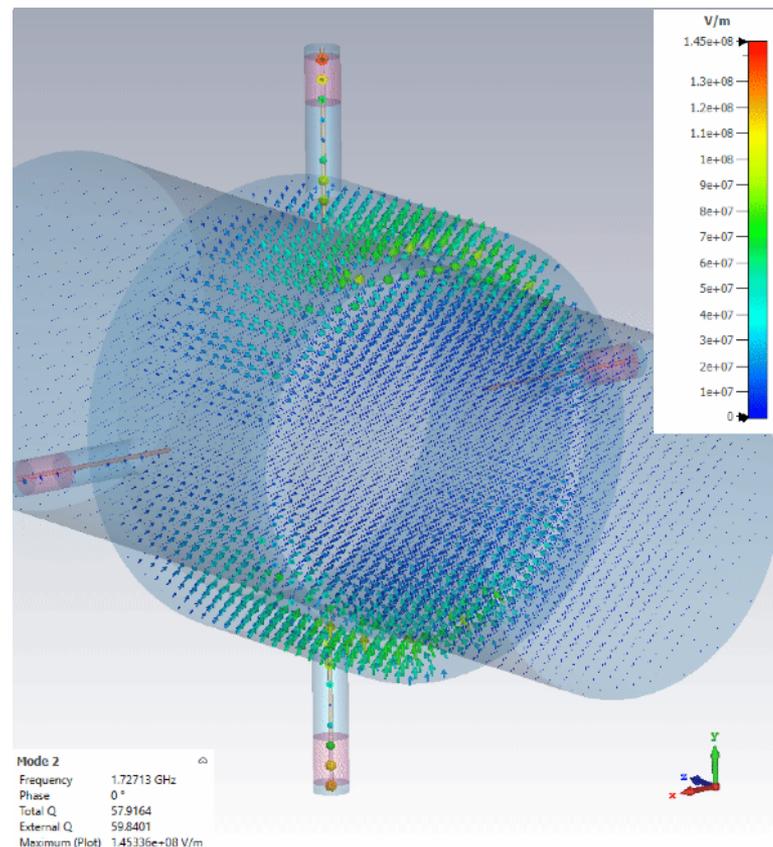


Figure: Design of cavity and feedthrough from cBPM from Saclay



III. Design studies of the cBPM

A) Geometry studies of the cBPM

• Parametric study

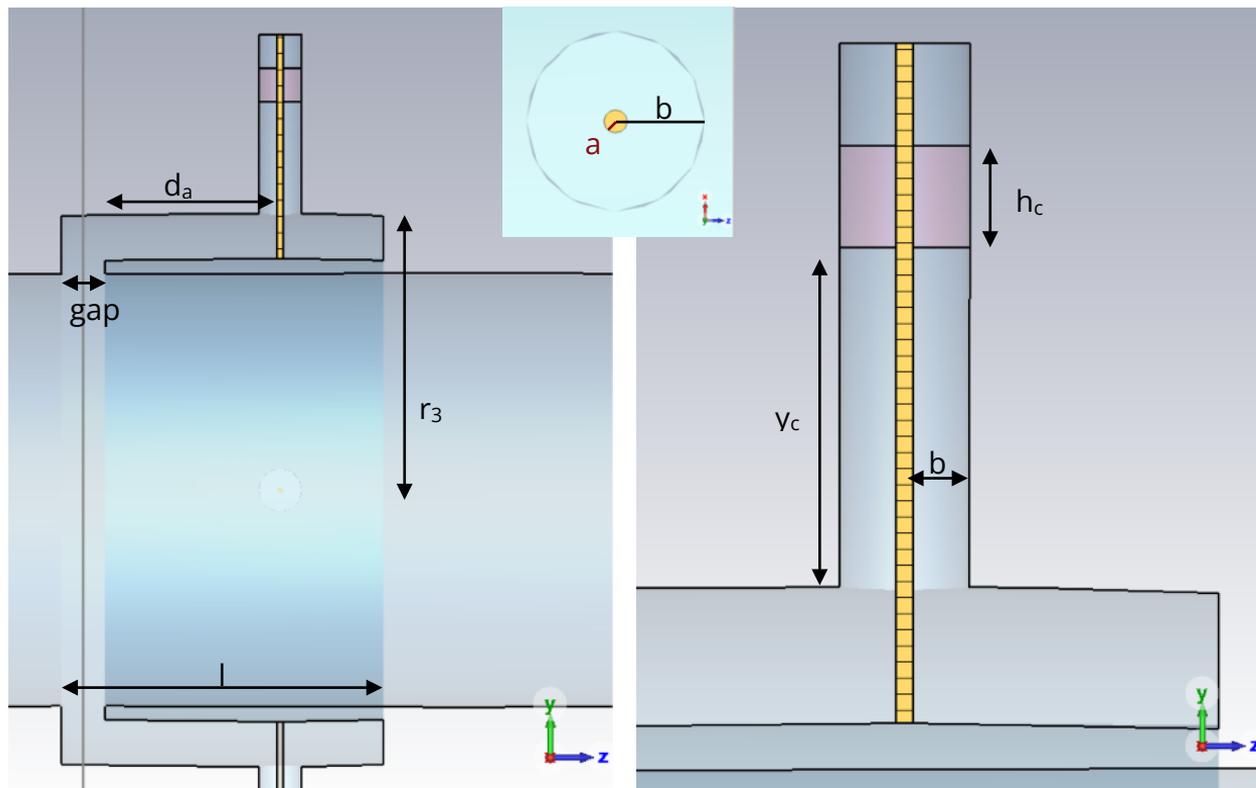


Figure: cBPM geometry dimensions

Preliminary conclusions:

Higher influence on Q_L (dipole) (and τ):

- \searrow when $l \nearrow$ (cavity length)
- \nearrow when $d_a \nearrow$ (antenna distance)
- \nearrow when $h_c \nearrow$ (thickness of seal)
- \searrow when $a \nearrow$ (radius of inner conductor) (but limited)

Higher influence on R/Q (dipole)
(sensitivity):

- \nearrow when $r_3 \nearrow$ (cavity aperture)
- \searrow when $l \nearrow$ (cavity length)

➔ Parameters usually affect all variables at the same time.
Need of careful selection.

III. Design studies of the cBPM

B) Inclusion of a perturbation in the cBPM

- Wakefield solver in CST

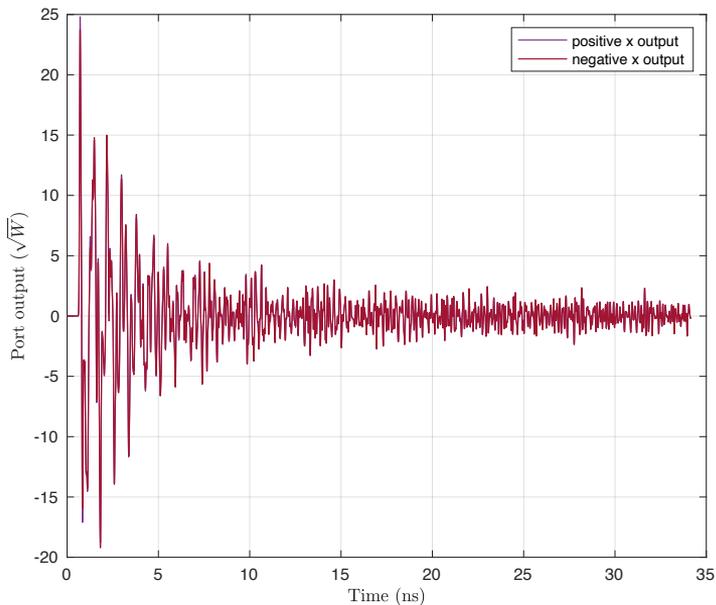


Figure: output signal from two opposite outputs on the wakefield simulation on CST

Evaluate the E and M fields under the presence of a beam and their response to different offsets

- ➔ Retrieve signal from the output ports and reconstruct beam dependence on the amplitude of the dipole mode

• Signal processing in MATLAB

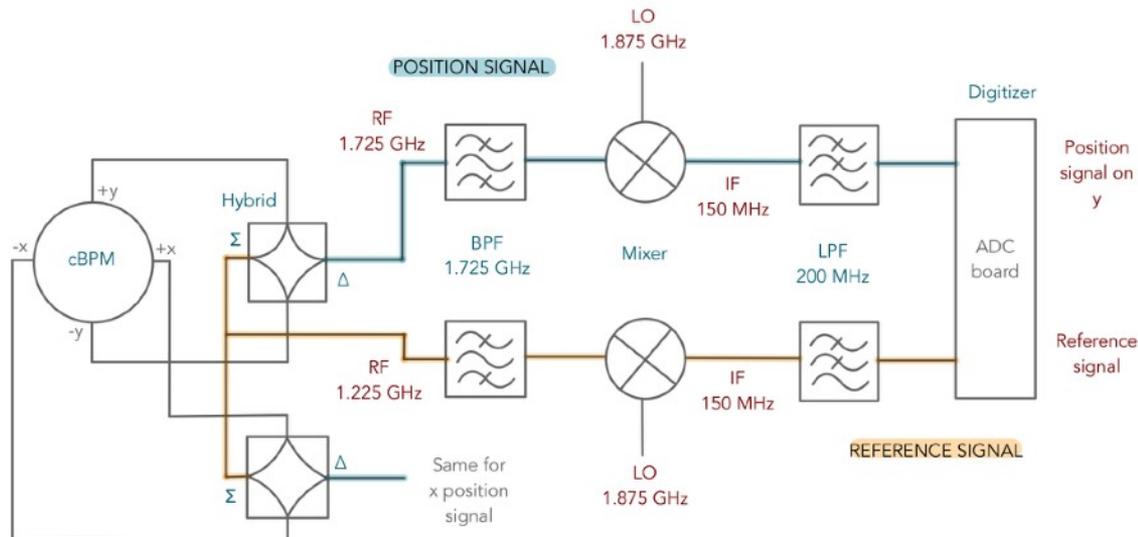


Figure: scheme of the provisional analog read-out system of the cBPM

III. Design studies of the cBPM

B) Inclusion of a perturbation in the cBPM

- **Signal processing in MATLAB**

- ❖ Extraction of information from both monopole and dipole modes from the same cavity.
- ❖ Hybrid coupler separates position and reference signal.
- ❖ The two signals are filtered at the dipole resonance frequency with BPF (butter-worth type)
 - filters leakage from hybrid
 - filters HOM
- ❖ Down-mixing of position and reference signal to 150 MHz
- ❖ Band-pass filter removes up-converted component and noise
- ❖ Digitizer of 600 MS/s

Retrieving maximum amplitude
 for range of offsets:

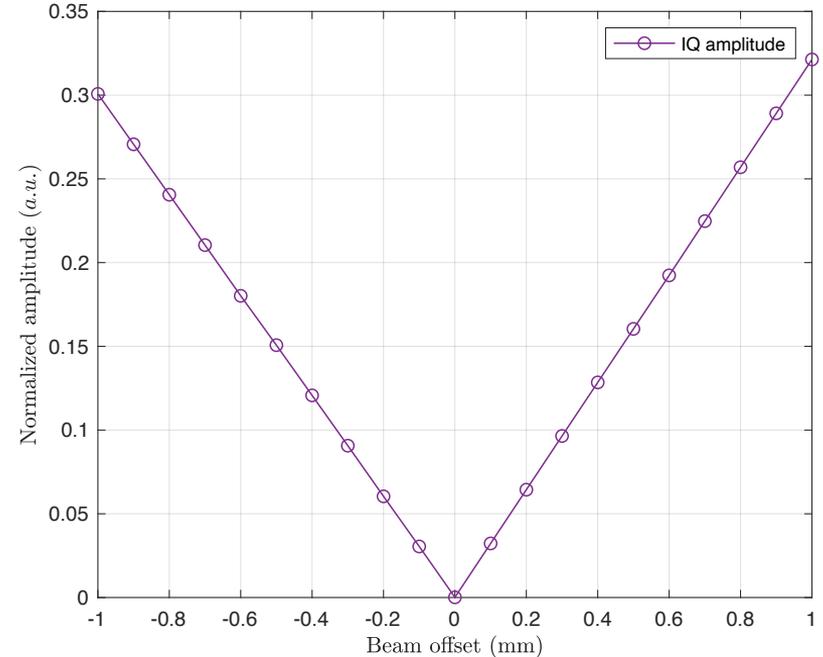


Figure: Position signal's amplitude dependence on δx

III. Design studies of the cBPM

C) BIR-ME 3D method

BI-RME 3D = Boundary Integral - Resonant Mode Expansion

Hybrid method that uses CST field results for a closed resonant cavity and allows to evaluate the RF power extracted at the output ports from the cavity when excited by a beam

- ➔ For a given operation frequency, the numerical method yields:
 - power consumed by the cavity P_c and power delivered to the waveguides (ports) P_w
 - output RF signal's amplitude and phase
 - external and loaded quality factors

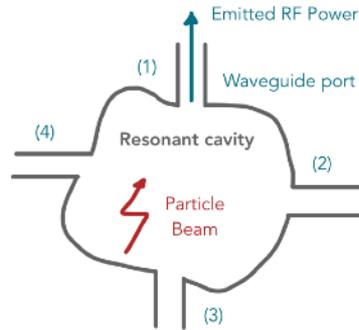
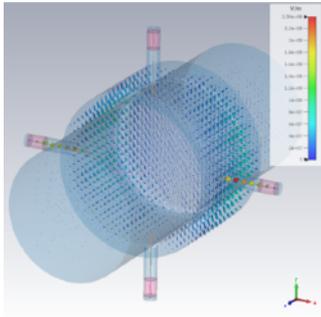
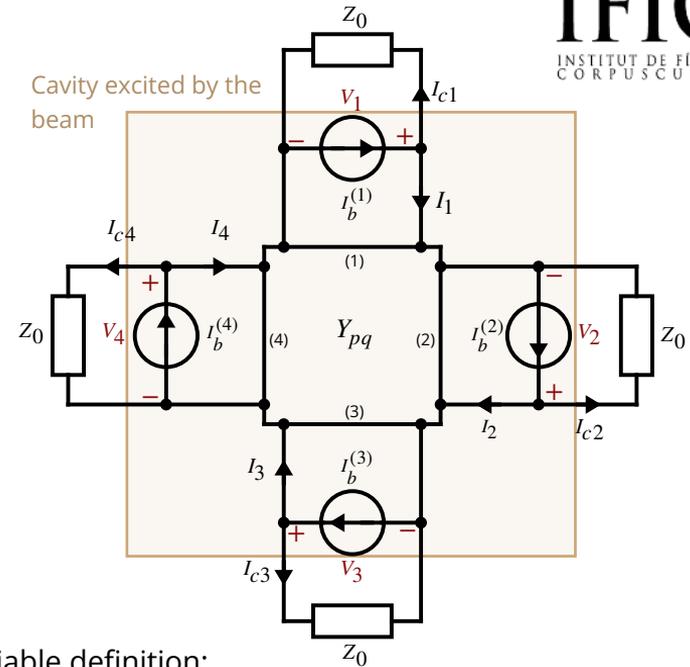


Figure: cBPM simulation in CST and representation for BIR-ME



Variable definition:

Z_0 impedance of coaxial output

V_i voltage at port (i)

$I_i = I_b^{(i)} - I_{ci}$ intensity at the cavity

$I_{ci} = V_i/Z_0$ intensity at the coaxial port

(Y_{pq}) is the Input admittance of the cavity

III. Design studies of the cBPM

C) BIR-ME 3D method

Intensity generated by the beam leading to port (i)

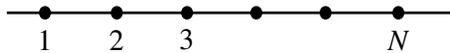
$$I_b^{(i)} = \sum_{m=1}^3 \frac{\kappa_m}{k^2 - \kappa_m^2} \int_{S^{(i)}} \vec{H}_m \cdot \vec{h}_{TEM}^{(i)} dS \int_V \vec{E}_m \cdot \vec{J}_b dV$$

Coupling cavity-port
Coupling beam-cavity

where

$$\kappa_m \simeq k_m \left(1 - \frac{1}{2Q_m} \right) + j \frac{k_m}{2Q_m} \quad \text{to consider Ohmic losses}$$

$$\vec{J}_b = \sum_{n=1}^N q_n \delta(\vec{r} - \vec{r}'_n) \vec{v}_n \quad \text{is the beam current density}$$



For a beam with a horizontal offset

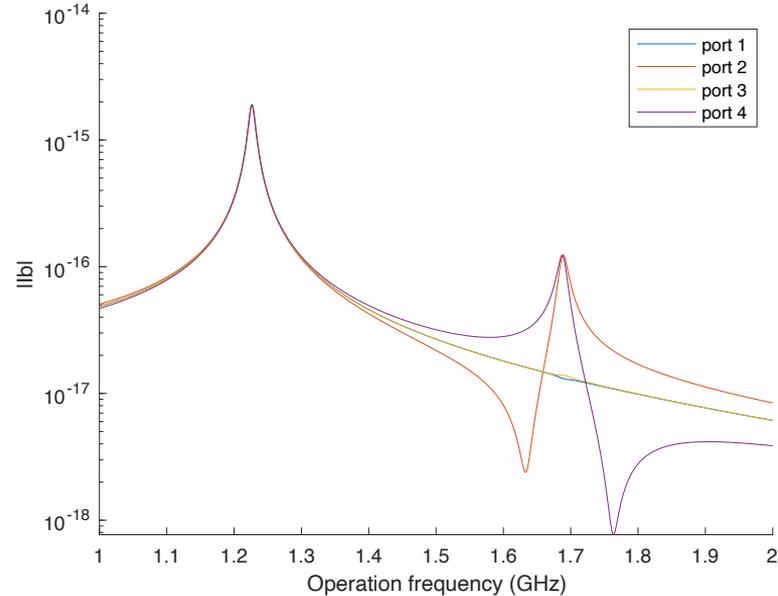


Figure 5: $|I_b^{(i)}|$ as a function of frequency for $\delta x = 5$ mm

cBPM developed by C. Simon (Saclay) enables bunch-to-bunch measurements at ILC with a resolution on the order of micrometers.

Methods employed to enhance the spatial resolution and meet the Main Linac requirements:

- The Saclay design is under evaluation to enhance BPM sensitivity and spatial resolution
- Simulation of the read-out system in MATLAB to assess the influence of all components on the overall system performance
- BIR-ME 3D method estimates the cBPM output signal with careful definition of the beam.

A preliminary plan is underway to develop a prototype integrating the SCQ and BPM assembly into a test cryostat.

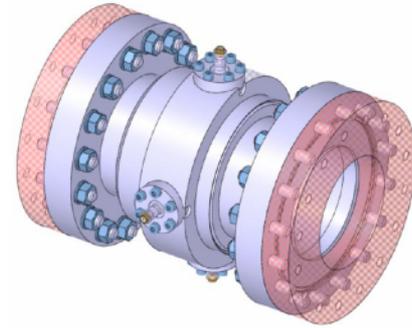


Figure: Design of cBPM from Saclay

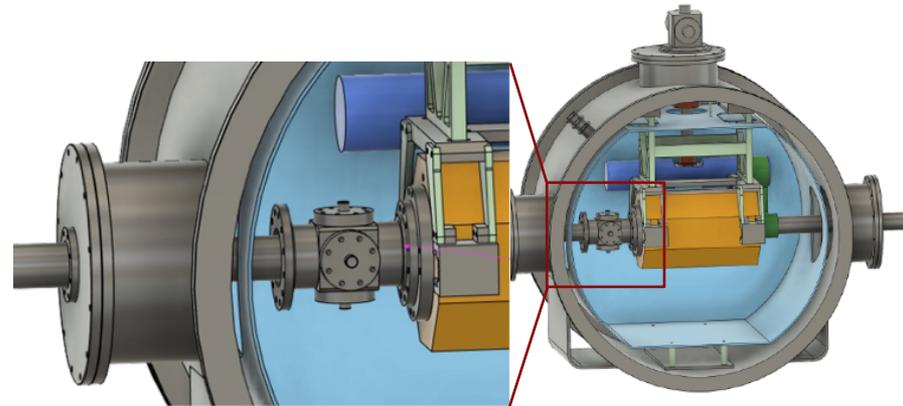


Figure: Cryostat accommodating BPM and SC quadrupole



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