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VNIVERSITAT DE VALÈNCIA

## Summary of 2023 work advances

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# Outline

- ❑ Limitation of conventional RF cavities
- ❑ Dielectric Assist Accelerating (DAA) cavity
- ❑ Dielectric Disk Accelerating (DDA) cavity
- ❑ Conclusion and next steps

# Limits of conventional accelerators

## ❑ Synchrotrons:

- Few RF cavities -> No need for very high electric fields
- Many bending magnets -> Energy loss by **synchrotron radiation**

$$\Delta E[\text{GeV}] = \frac{6.034 \times 10^{-18}}{\rho[\text{m}]} \left( \frac{E[\text{GeV}]}{m_0[\text{GeV}/c^2]} \right)^4$$

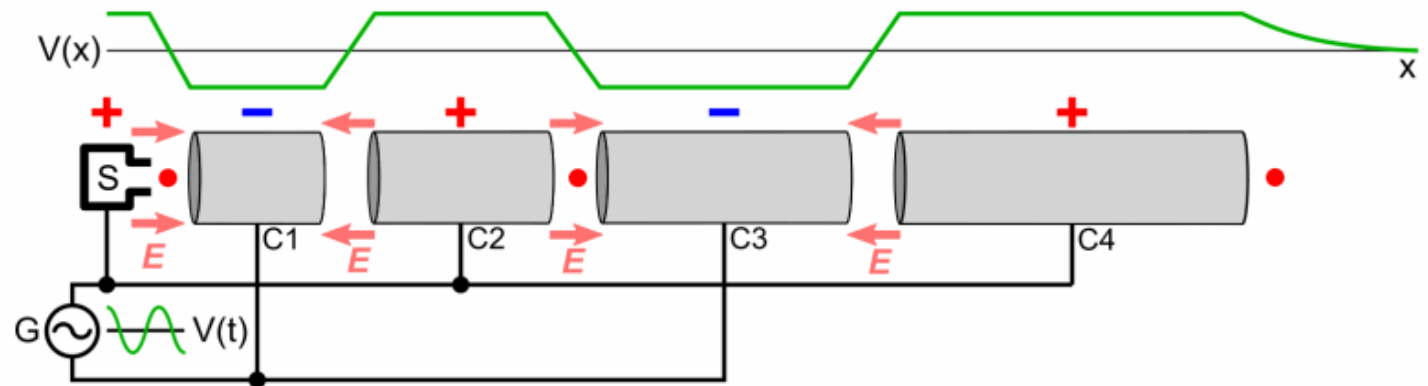
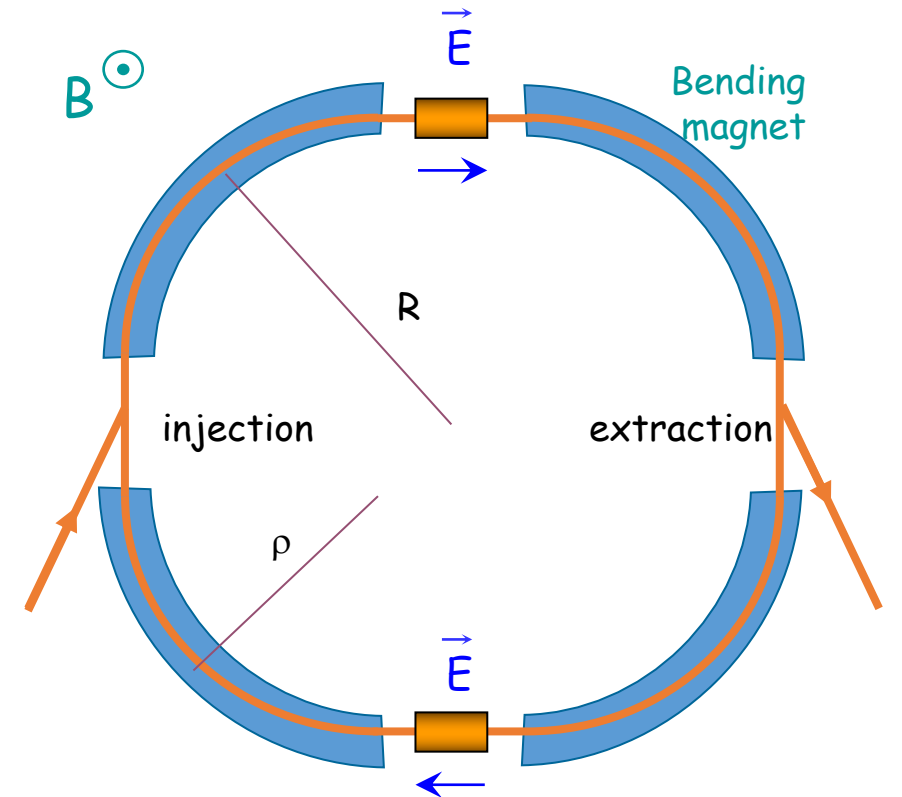
$m_0$ : rest mass  
 $E$ : energy  
 $\rho$ : radius of curvature

Key constraint for **light particles**

## ❑ Linear accelerators

- Few bending magnets -> No energy loss by synchrotron radiation
- Many RF cavities -> High accelerating gradient or large machines.

Gradients limited around **100 MV/m**  
due to **surface breakdown**

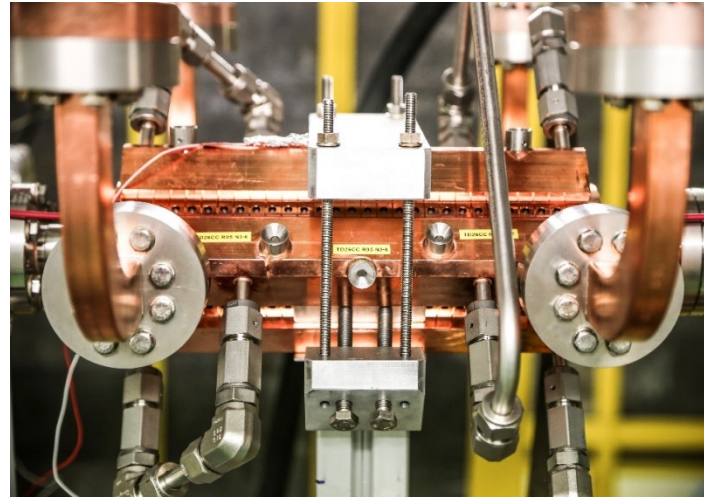


# Surface breakdown phenomenology

RF signals

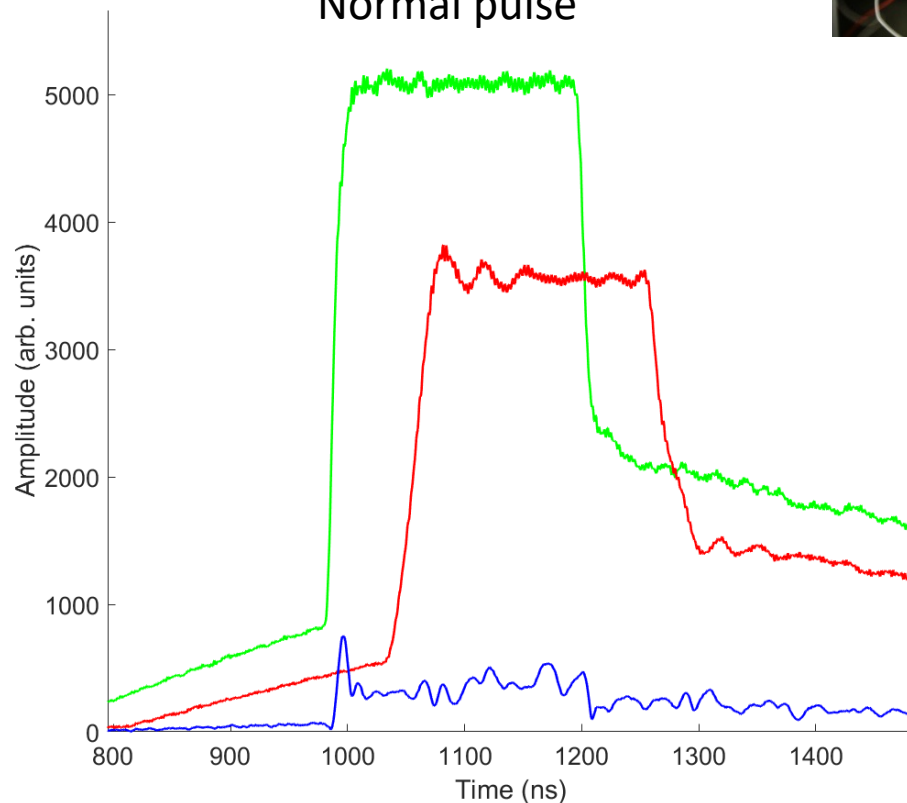
incident power

reflected power

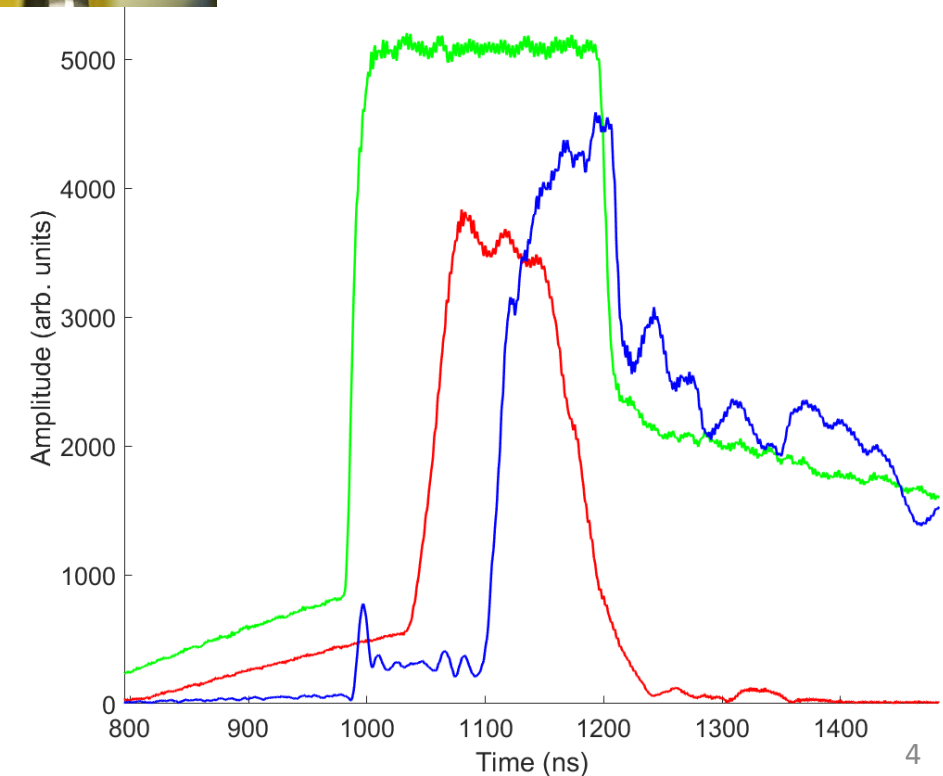


transmitted power

Normal pulse



Breakdown pulse



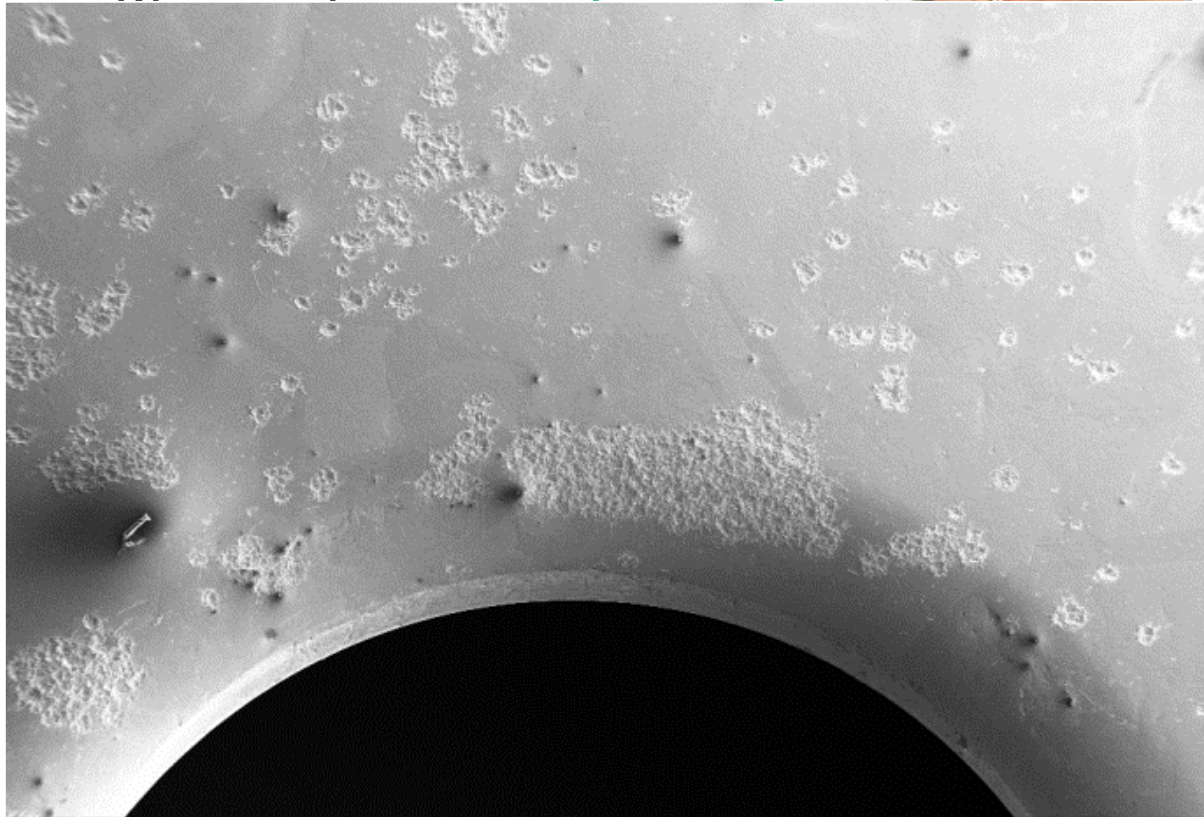




# Surface breakdown phenomenology

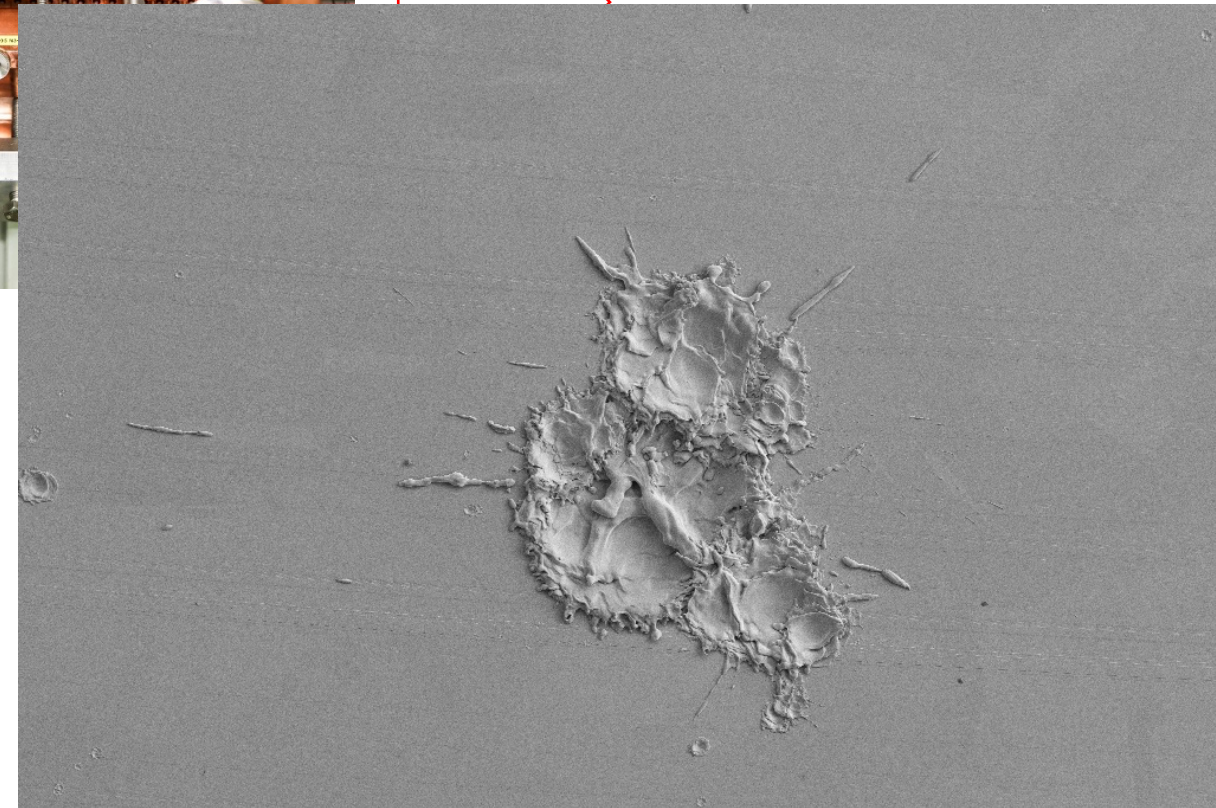
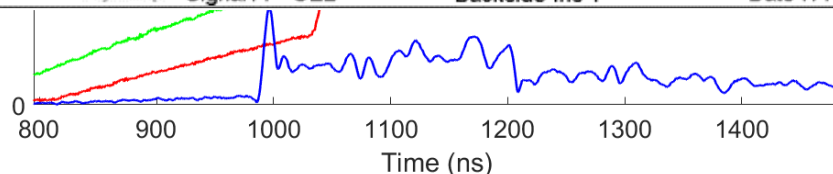
incident power





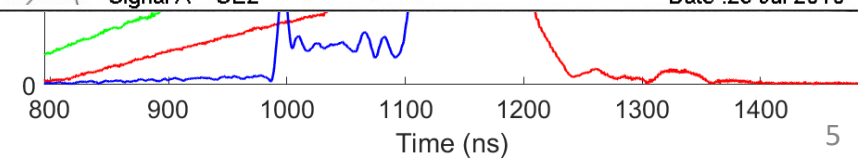
transmitted power



200  $\mu\text{m}$   EHT = 5.00 kV  
WD = 17.3 mm T18 KEK/SLAC  
Signal A = SE2 part B Tilt 30°  
Mag = 18 X  
Ana T. Perez Fontenla  
Date :11 Mar 2011 

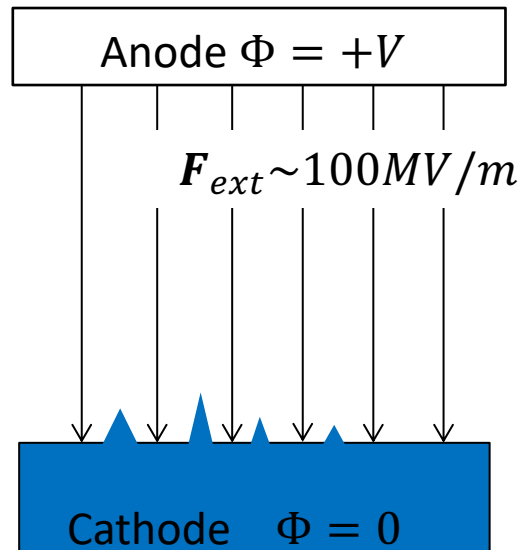


20  $\mu\text{m}$   EHT = 3.00 kV  
WD = 5.1 mm DC-Spark sample Cu(47)  
Signal A = SE2 Spot 7 (4.65)  
Mag = 200 X  
Markus Aicheler  
Date :29 Jul 2010 

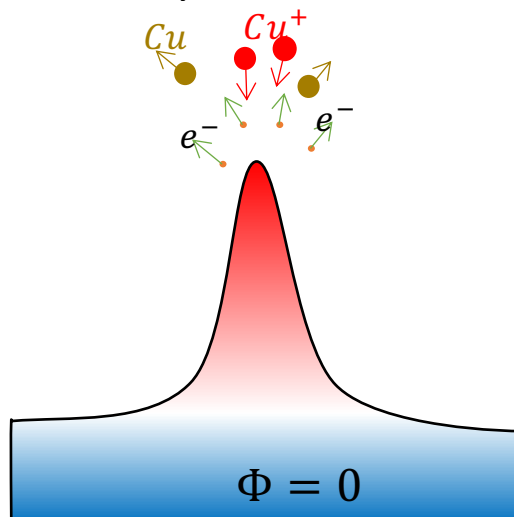


# Surface breakdown initiation

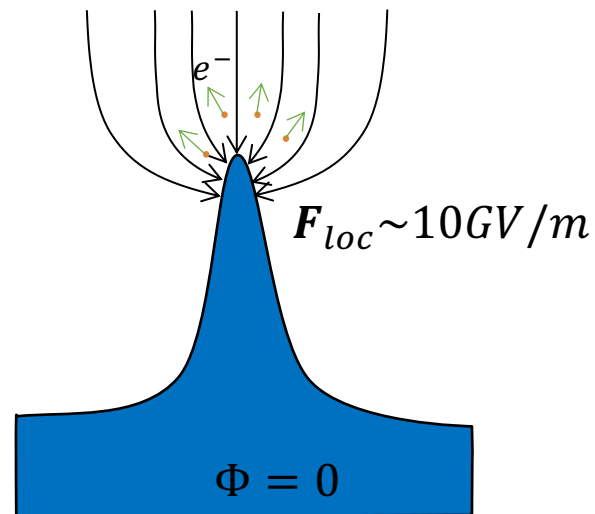
Stage 0: Flat surface



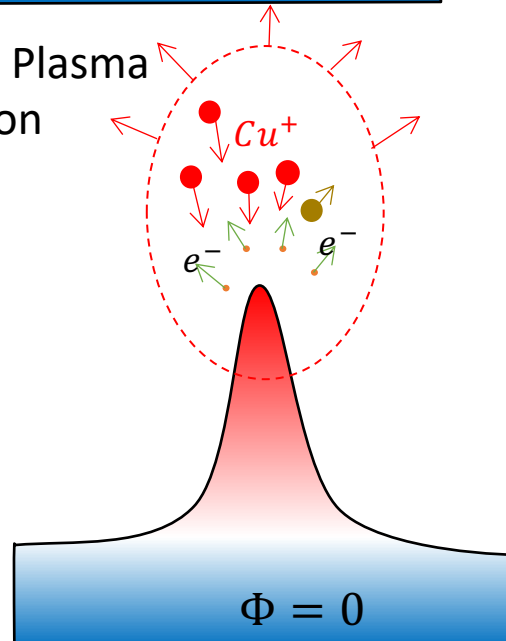
Stage 3: Ionization runaway & Plasma onset



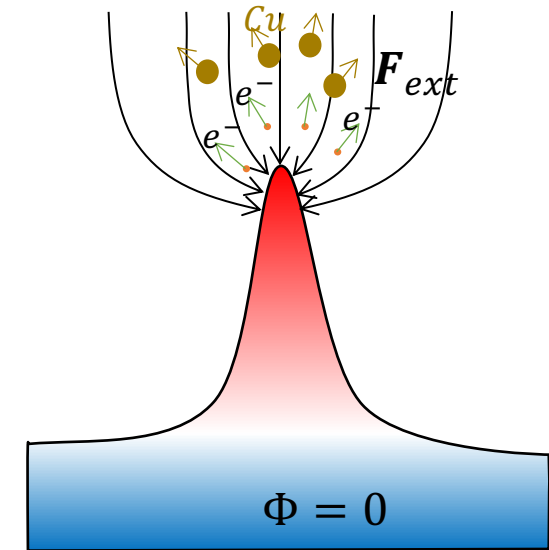
Stage 1: Field emission



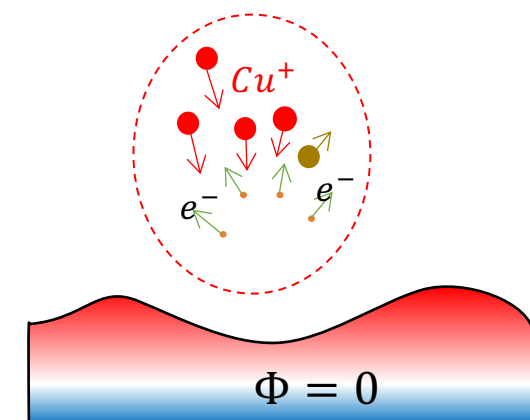
Stage 4: Plasma expansion



Stage 2: Field emitter Thermal Runaway

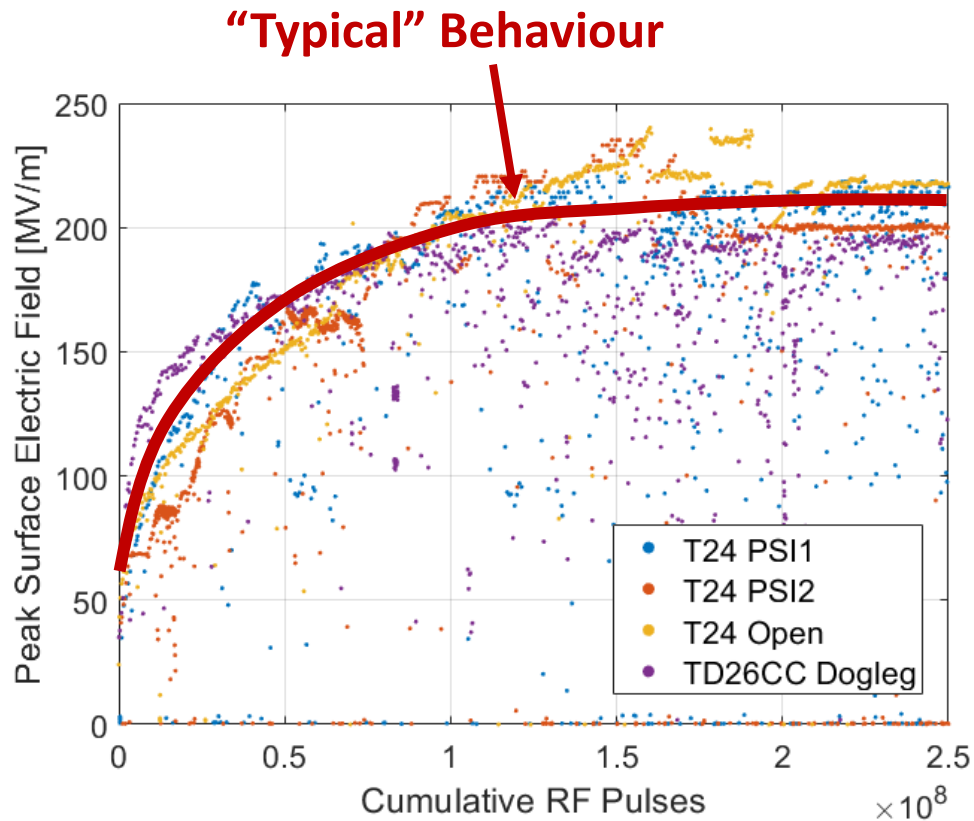


Stage 5: Burning arc, crater formation



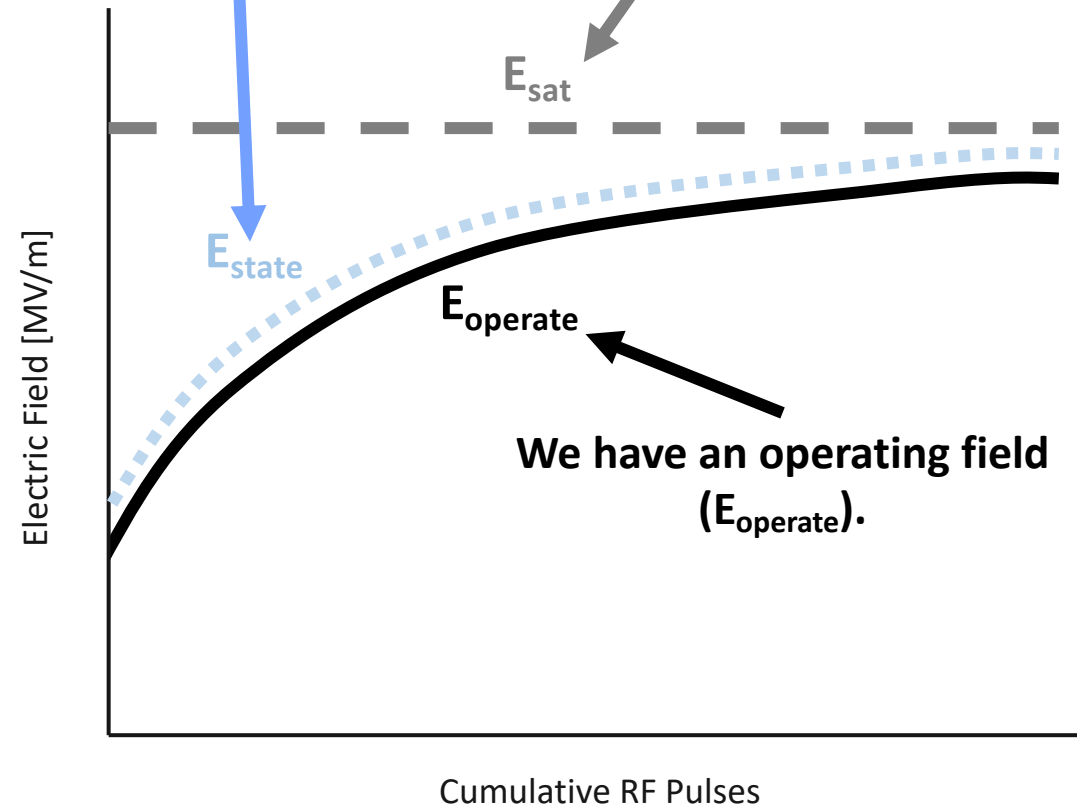
# RF Conditioning

- Start at low electromagnetic field level.
- Gradually increase field keeping a safe breakdown rate.
- Reach field saturation.



The field level to which the device has been conditioned ( $E_{\text{state}}$ ).

There is a saturation point for  $E_{\text{state}}$  for a given material ( $E_{\text{sat}}$ ).

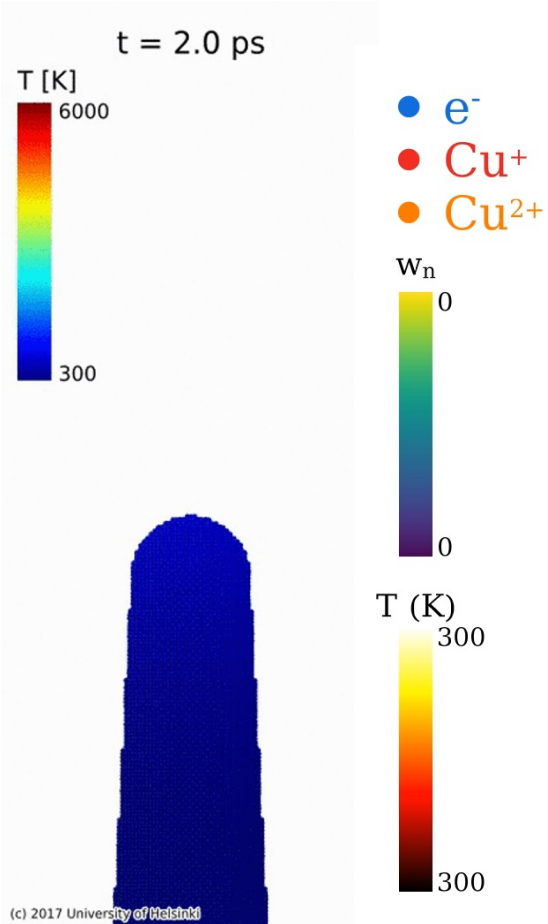




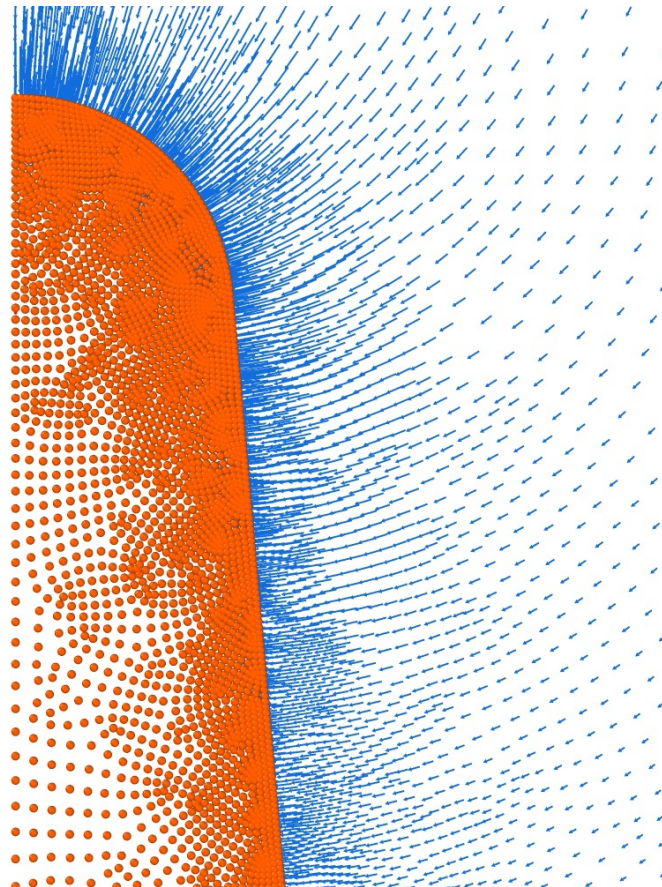
# Complexity of surface breakdown

- Simulation: ns, nm, simple systems

## Molecular Dynamics

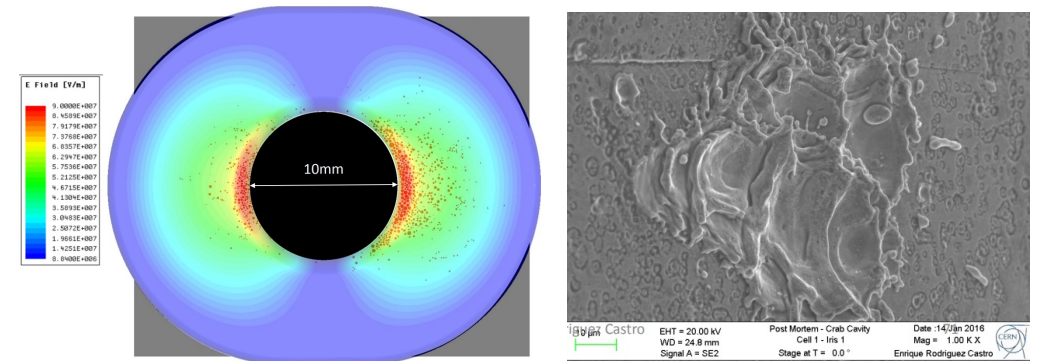


## FEMOCS

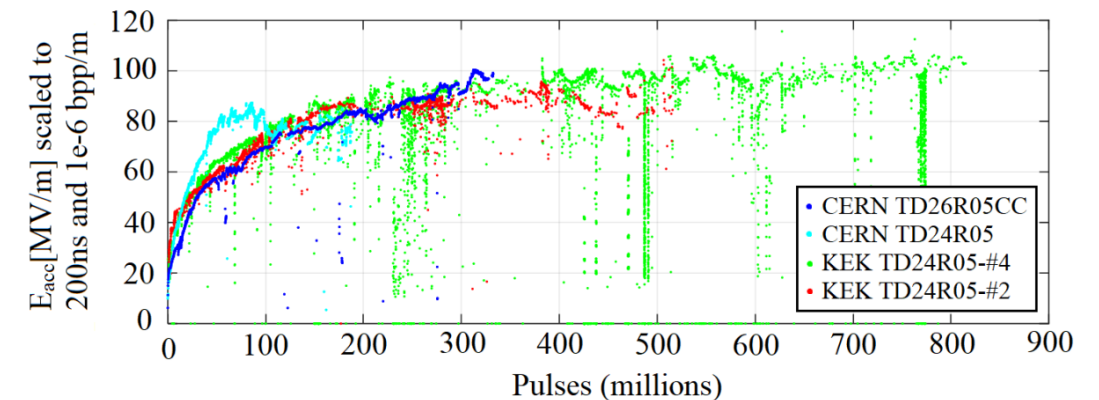


- Experiment: sec, mm, complex systems

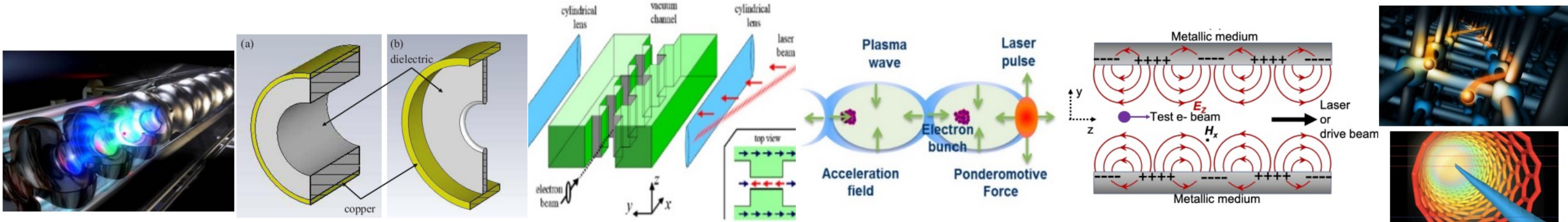
## Post-mortem analysis



## Conditioning curves & history



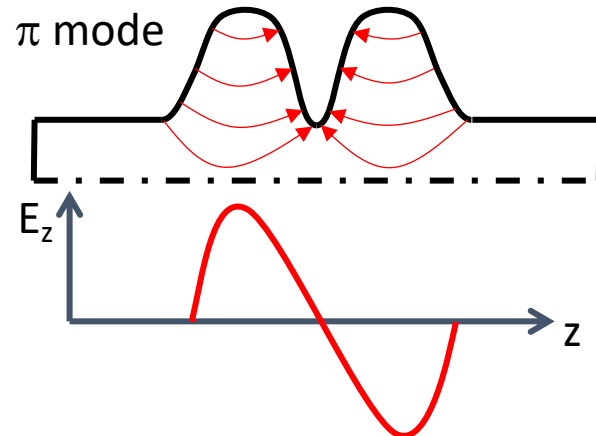
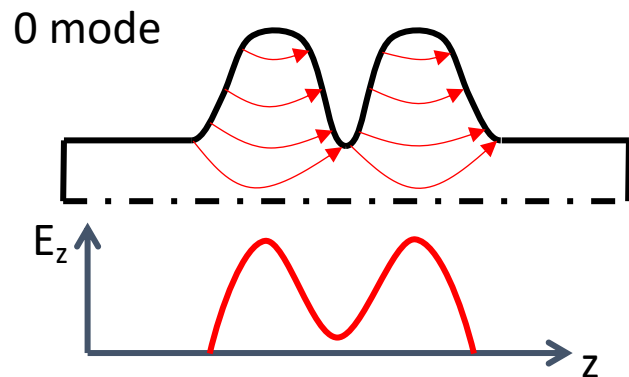
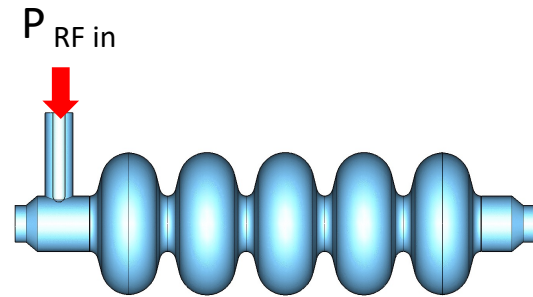
# Novel accelerators



	Conventional RF cavities	Dielectric Loaded RF cavities	Dielectric laser – driven acceleration (DLA)	Plasma / Laser wakefield acceleration (PWFA / LWFA)	Plasmonic acceleration	Solid-state plasma Wakefield acceleration
Based on	Normal / superconducting cavities	Metallic and dielectric	Quartz / silicon structure	Gaseous plasma	Excitation of plasmons	Crystals, nano-channels, Carbon Nanotubes
Max. longitudinal electric field	~100 MV/m	~100 MV/m (?)	~10 GV/m	~100 GV/m	~100 GV/m	~1 – 100 TV/m (prediction)
Limitation	Surface breakdown	Multipactor and breakdown (?)	Damage threshold	Wave breaking	Beam matching with excited plasmonic oscillations	Wave breaking

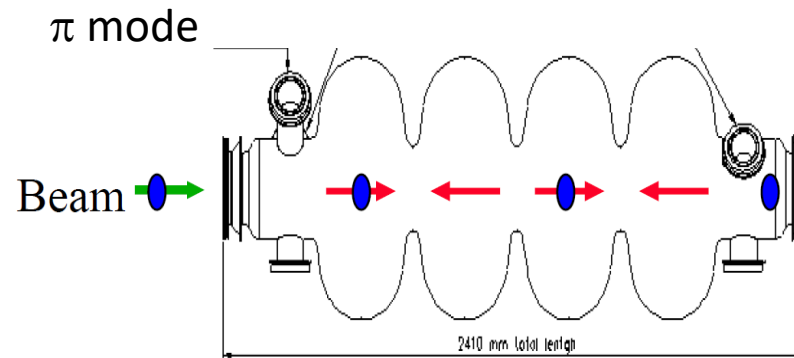
Hard to get high quality beams

# Standing Wave Acceleration Cavities

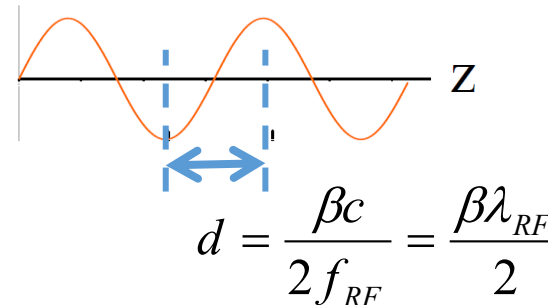


Cylindrical single (or multiple cavities) working on the  $TM_{010}$ -like mode are used

Synchronization condition



Electric field  
(at time  $t_0$ )



$\beta$ : particle velocity  
 $d$ : distance between cells  
 $f_{RF}$ : RF frequency  
 $c$ : speed of light in vacuum

Figures of merit:

- Shunt impedance: efficiency of the acceleration mode.

$$R = \frac{\hat{V}_{acc}^2 T^2}{P_{diss}} [\Omega]$$

NC cavity  $R \sim 1M\Omega$  SC cavity  $R \sim 1T\Omega$

- Quality factor: efficiency to store RF energy .

$$Q = \omega_{RF} \frac{W}{P_{diss}}$$

NC cavity  $Q \sim 10^4$  SC cavity  $Q \sim 10^{10}$

- R/Q: pure geometric qualification factor.

$$\frac{R}{Q} = \frac{\hat{V}_{acc}^2 T^2}{\omega_{RF} W} \sim 100 \Omega$$

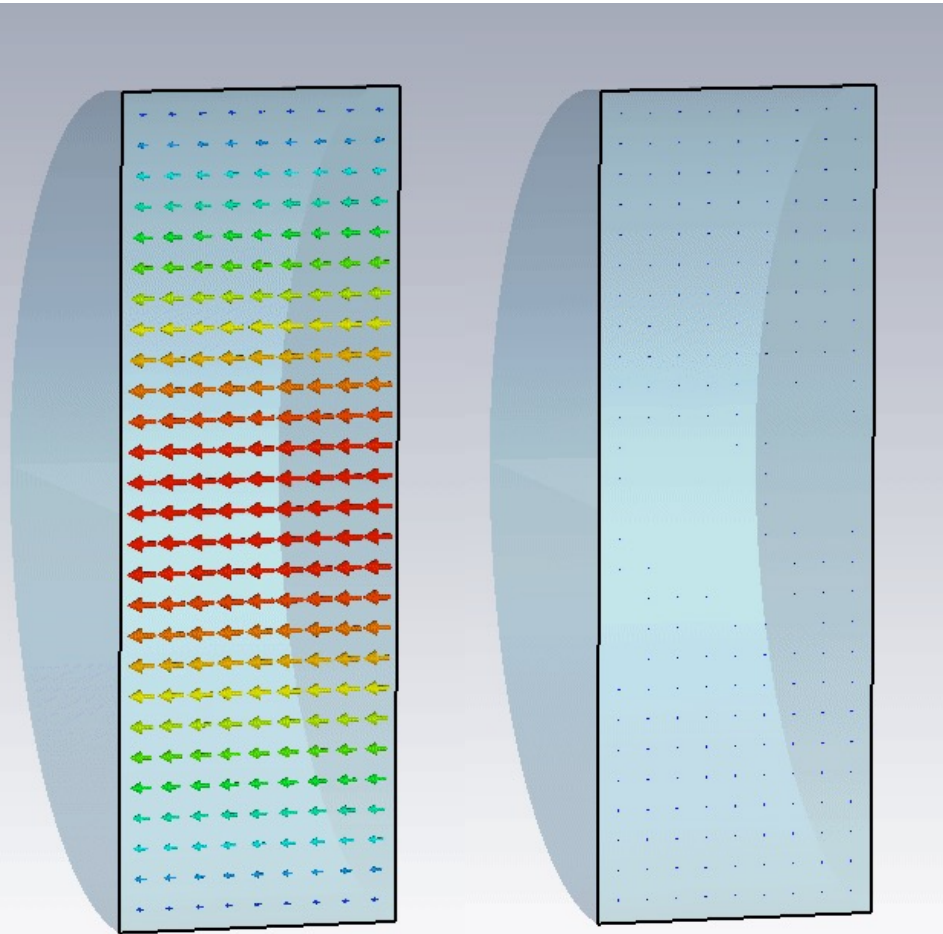


# Copper structure single cell

Pillbox cavity  $TM_{010}$

Electric field

Magnetic field



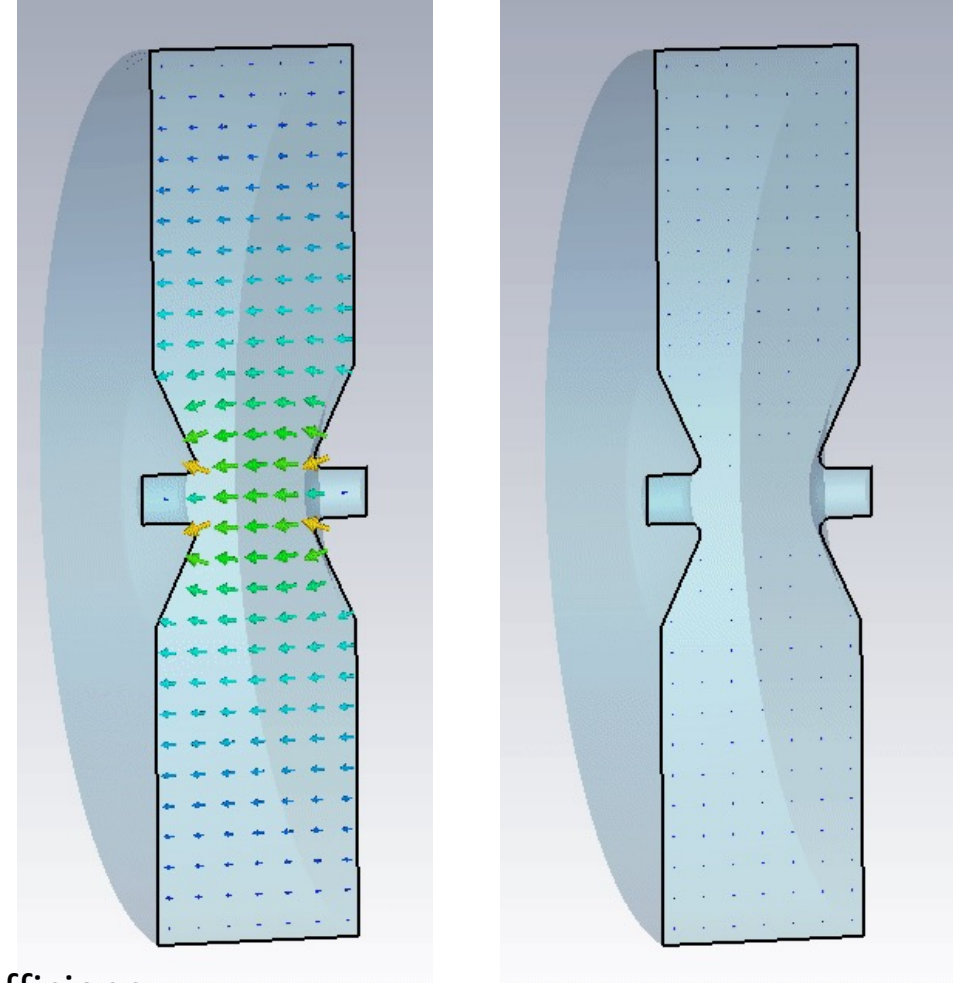
Optimization



Accelerating cavity mode  $TM_{010}$

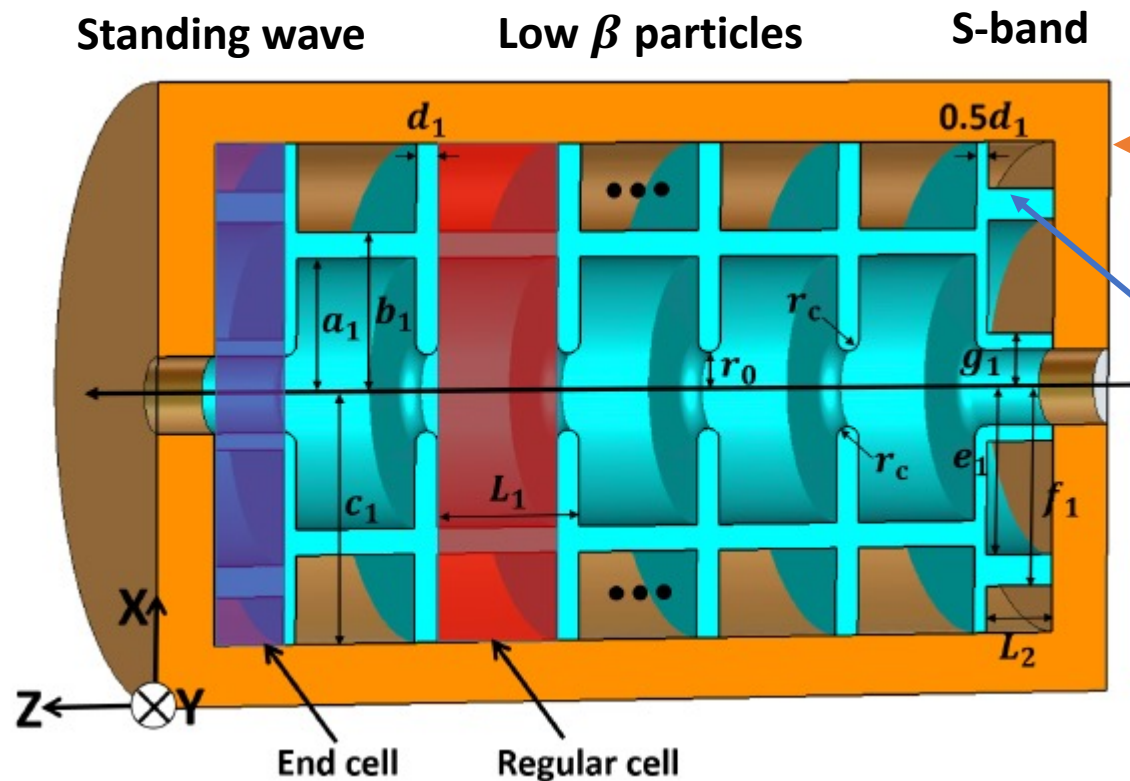
Electric field

Magnetic field



- High losses in metallic walls: low RF efficiency.
- High peak electric field in metal: field emission and RF breakdown.

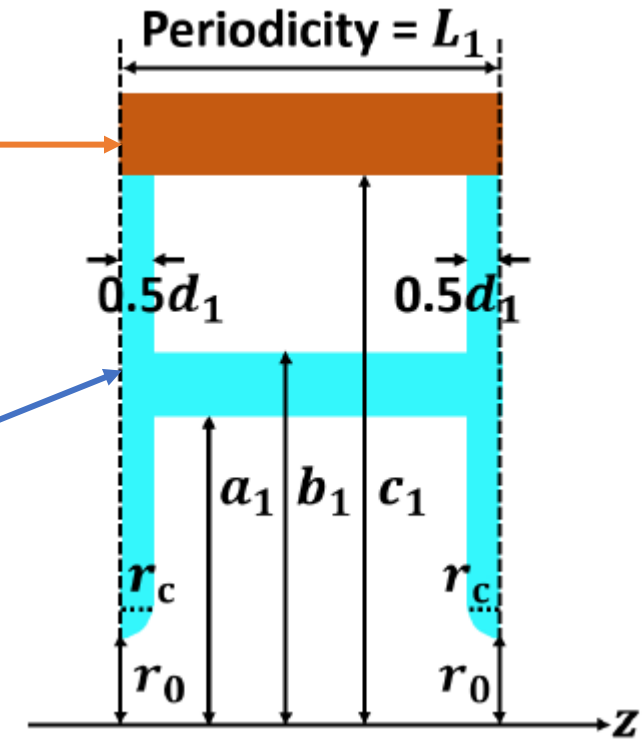
# Dielectric Assist Accelerating (DAA) cavity



Copper

Dielectric:

- High  $\epsilon_r$
- Low  $\tan \delta$



D. Satoh, M. Yoshida, and N. Hayashizak, "Dielectric assist accelerating structure." *Physical Review Accelerators and Beams*, vol. 19, 1, pp. 1011302, 2016  
Investigations Into X-Band Dielectric Assist Accelerating Structures for Future Linear Accelerators. Yelong Wei, Alexej Grudiev.

TABLE I  
LIST OF DIELECTRICS STUDIED IN THE OPTIMIZATION

Material	Acronym	$\epsilon_r$	$\tan \delta$
CVD Diamond	Diamond	5.7	$10^{-4}$
MgO	D9	9.64	$6 \times 10^{-6}$
MgTiO <sub>3</sub>	D16	16.66	$3.43 \times 10^{-5}$
BaTiO <sub>x</sub>	D50	50.14	$8 \times 10^{-5}$

Working under  $TM_{02} - \pi$  mode:

- High  $Q_0$ .
- Dielectric helps to decrease cavity size.
- Low electric field in metal.
- Axial symmetry

Resonant frequency for the mode depends on the combination of  $a_1, b_1, c_1$



# Energy range for hadrontherapy

$$Q = \omega_{RF} \frac{W}{P_{diss}}$$

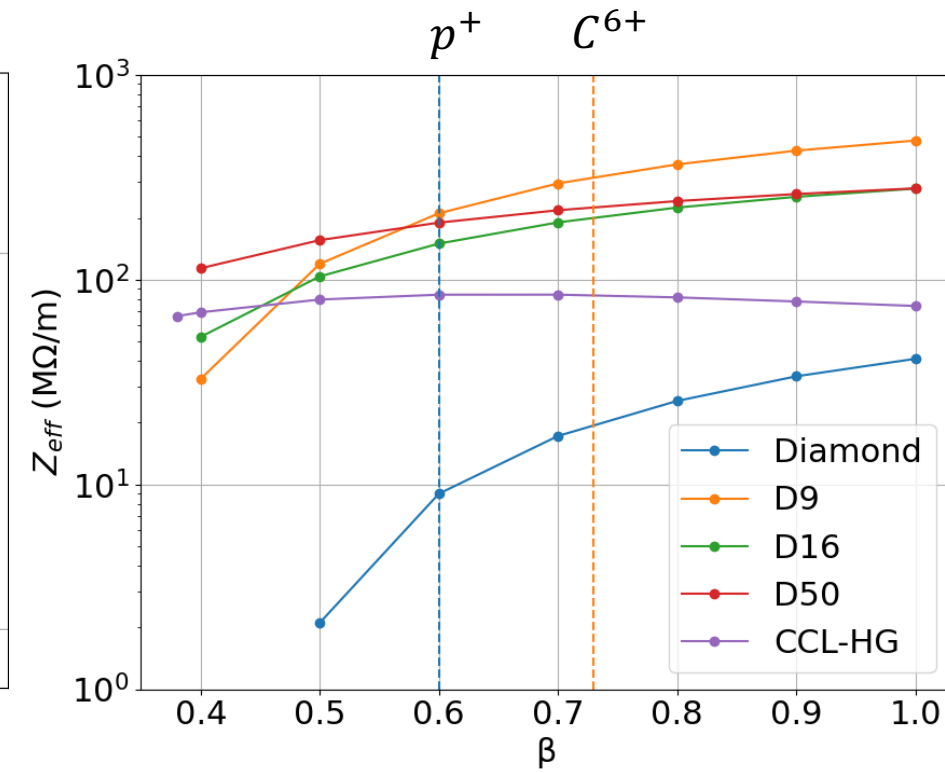
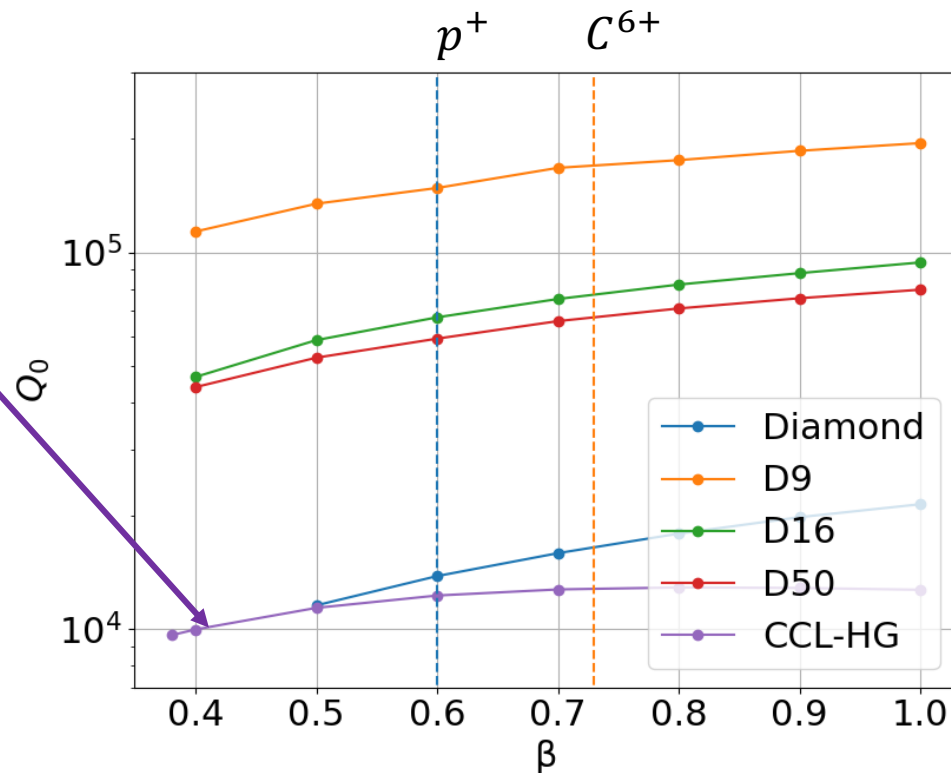
$$R = \frac{\hat{V}_{acc}^2 T^2}{P_{diss}} [\Omega]$$

- Protons: 70 – 230 MeV  $\rightarrow \beta : 0.37 - 0.6$
- $^{12}\text{C}^{6+}$ : 100 – 430 MeV/u  $\rightarrow \beta : 0.43 - 0.73$

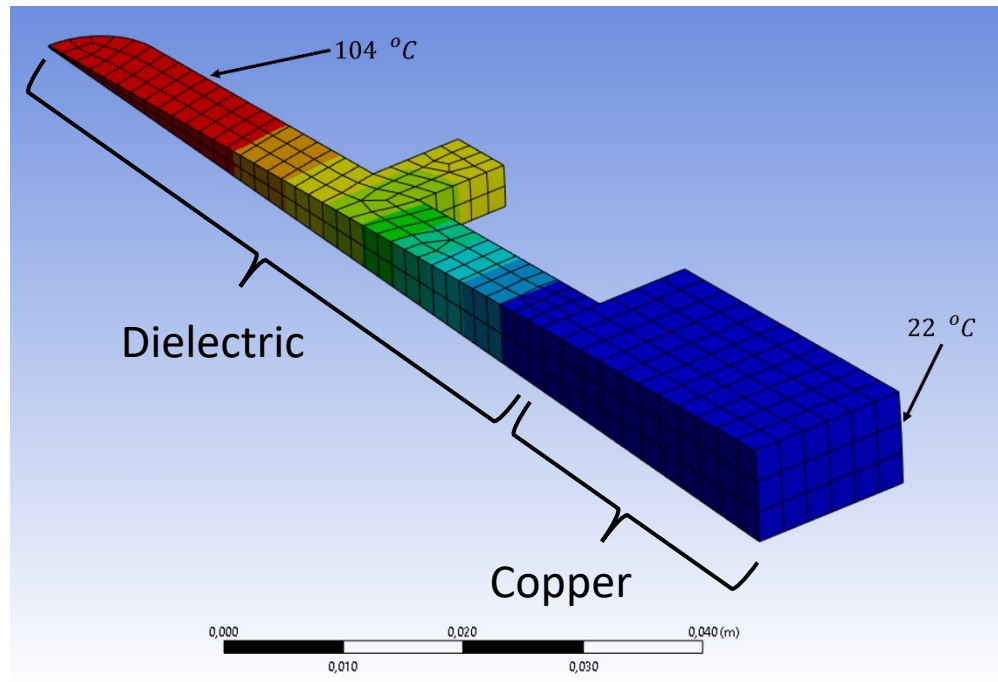
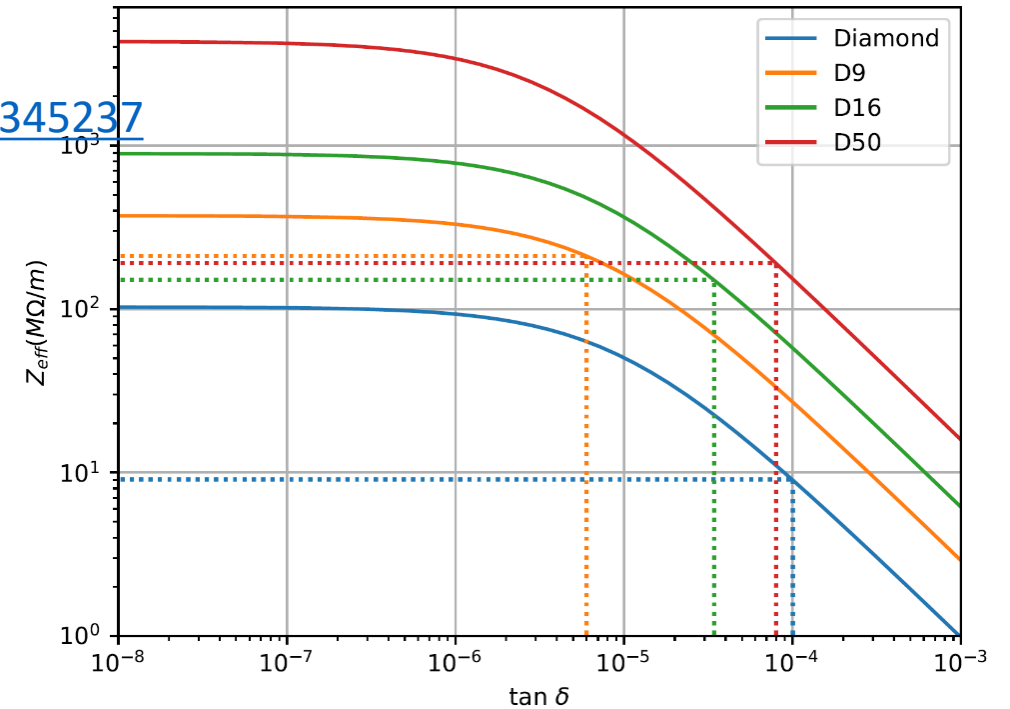
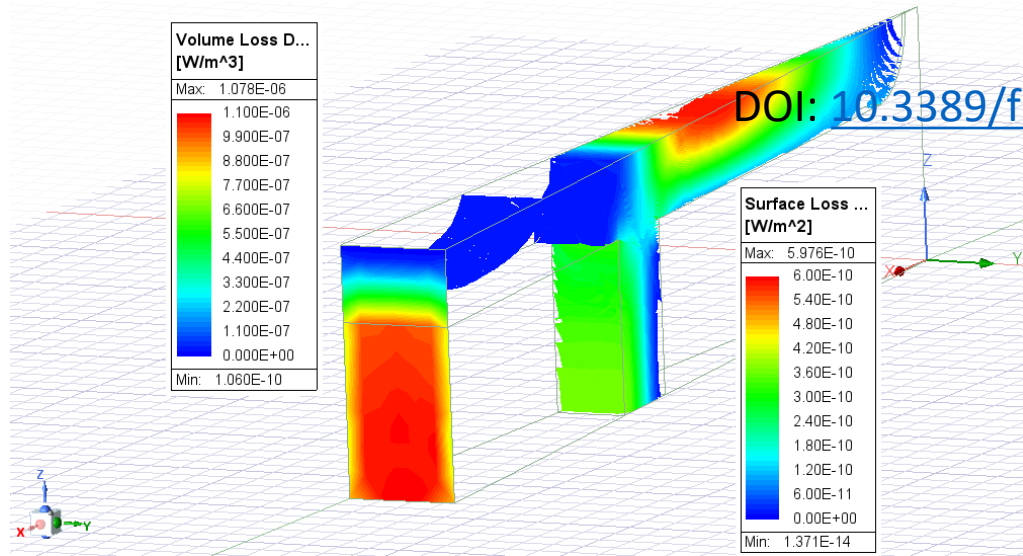
Bencini, V. (2020). *Design of a novel linear accelerator for carbon ion therapy* (Doctoral dissertation, Rome U.).

□ Design compared with a **normal cooper cavity** for proton therapy (purple).

□ Factor 1.5 to 100 improvement depending on the material and characteristics.



# Challenges



## Challenges

- ☐ Finding the right material (high  $\epsilon_r$  and small  $\tan \delta$ ).
- ☐ Mechanize the geometry within the tolerances required.
- ☐ Mitigation of non-linear EM phenomena such as multipactor.
- ☐ Field singularities at triple point junctions.
- ☐ Cooling of the ceramic

**Volume Loss D...  
[W/m<sup>3</sup>]**

Max: 1.078E-06

1.100E-06  
9.900E-07  
8.800E-07  
7.700E-07  
6.600E-07  
5.500E-07  
4.400E-07  
3.300E-07  
2.200E-07  
1.100E-07  
0.000E+00

Min: 1.060E-10



TYPE Original Research  
PUBLISHED XX XX 2024  
DOI 10.3389/fphy.2024.1345237

 Check for updates

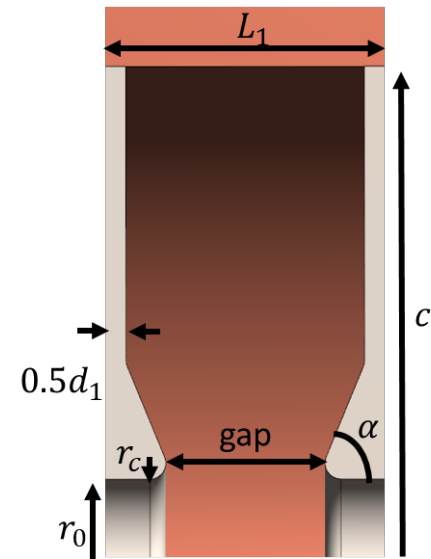
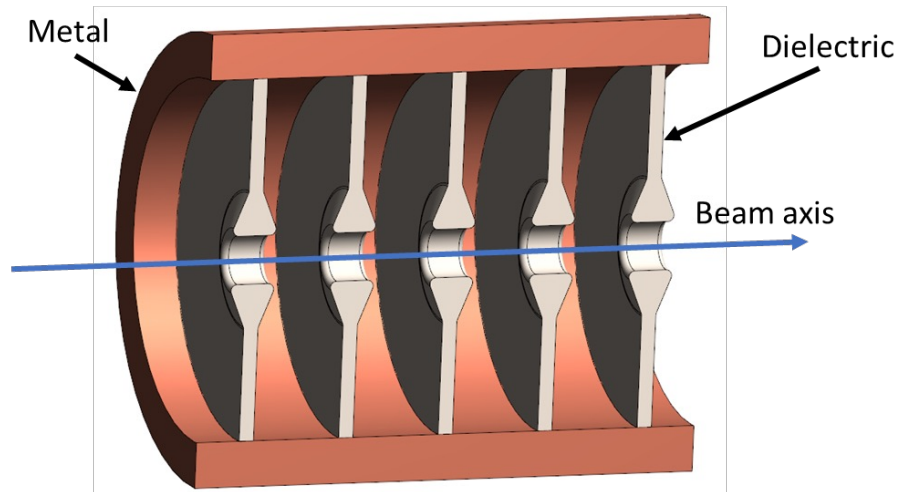
**Q7**

dielectric assist accelerating (DAA) structures, radio frequency (RF), LINAC, Q8



# Dielectric Disk Accelerating (DDA) cavity

□ **Goal:** design a prototype to test dielectric cavities.

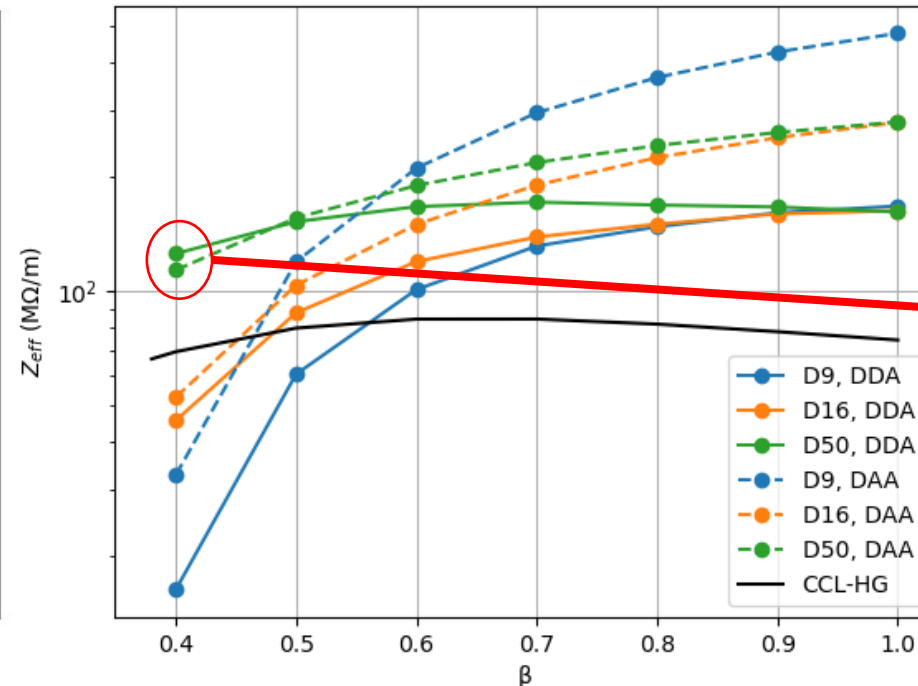
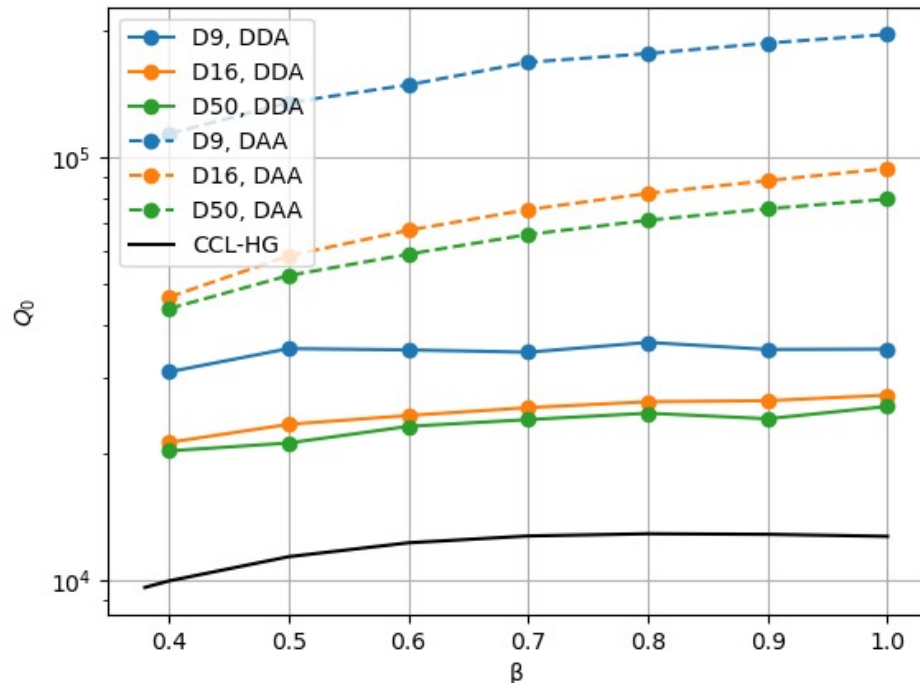


Advantages:

- Simpler geometry
- Less sensitive to material

Challenges:

- Multipactor
- Fabrication



DDA structure with **D50** material for  $\beta = 0.4$  is a promising solution.

# Dielectric Disk Loaded Accelerating (DDA) Cavity

## Pros:

- Coupling can be adjusted easily
- Low coupling to other modes
- Low magnetic field in coupling cavity
- Low electric field on coupling metallic iris.
- More symmetry.

## Cons:

- Mode launcher needed.

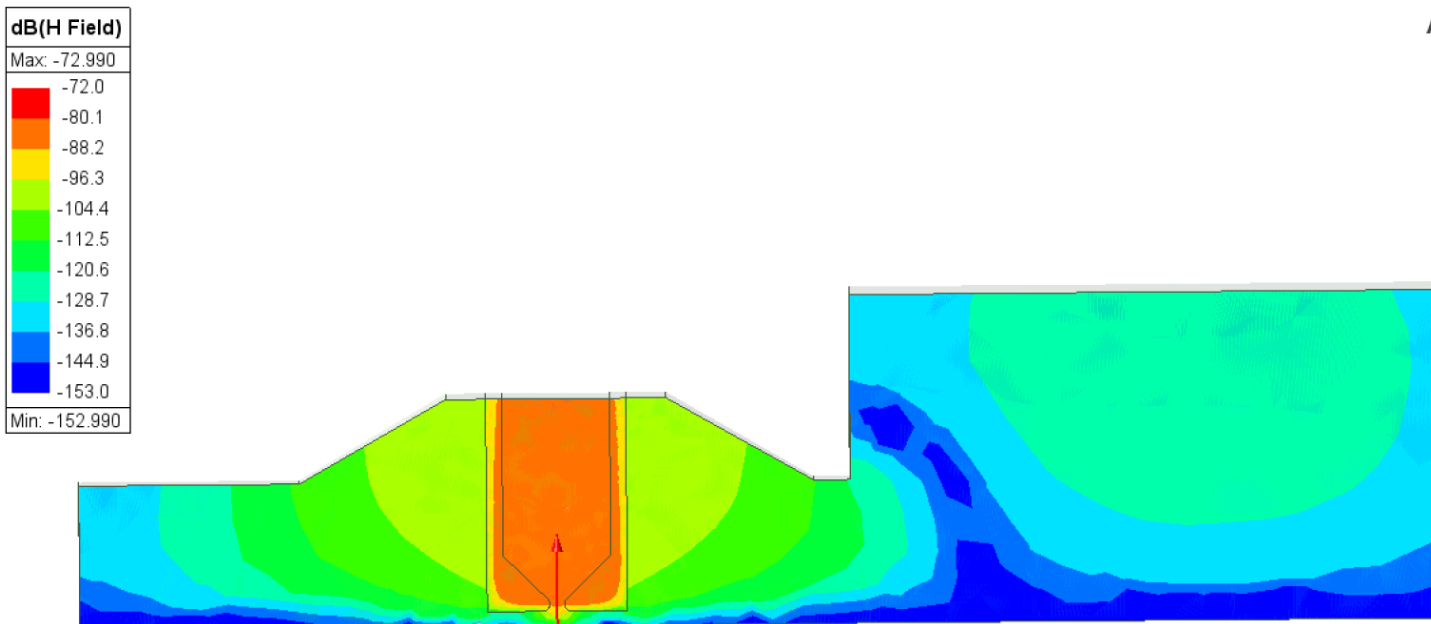
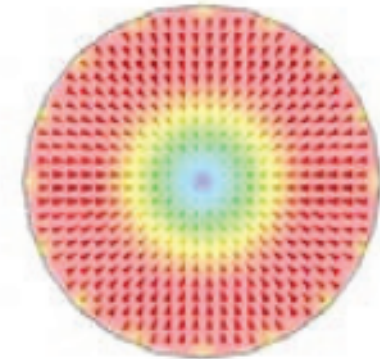
Laboratory output:  
Rectangular waveguide

$TE_{10}$



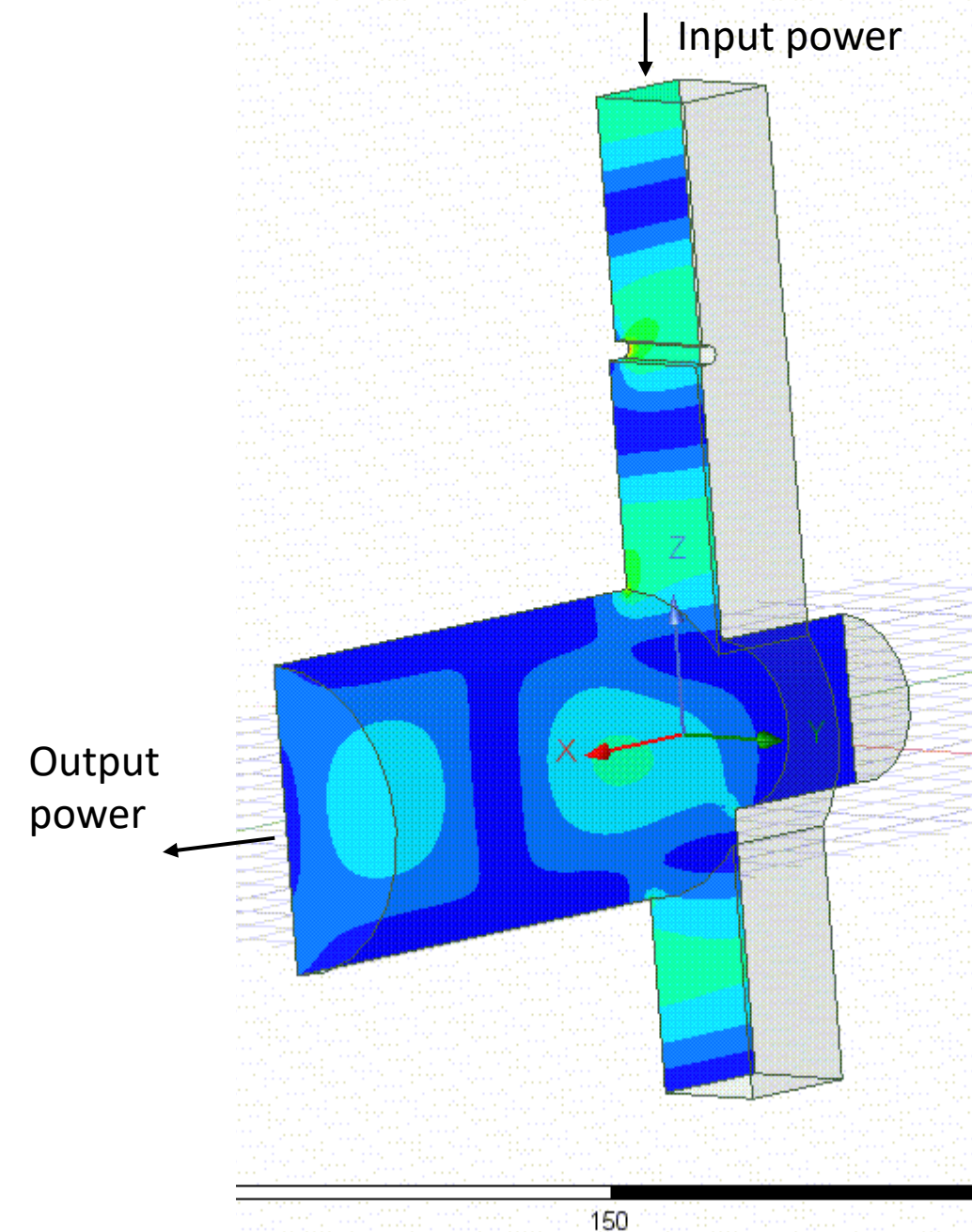
Cavity input:  
Circular waveguide

$TM_{01}$

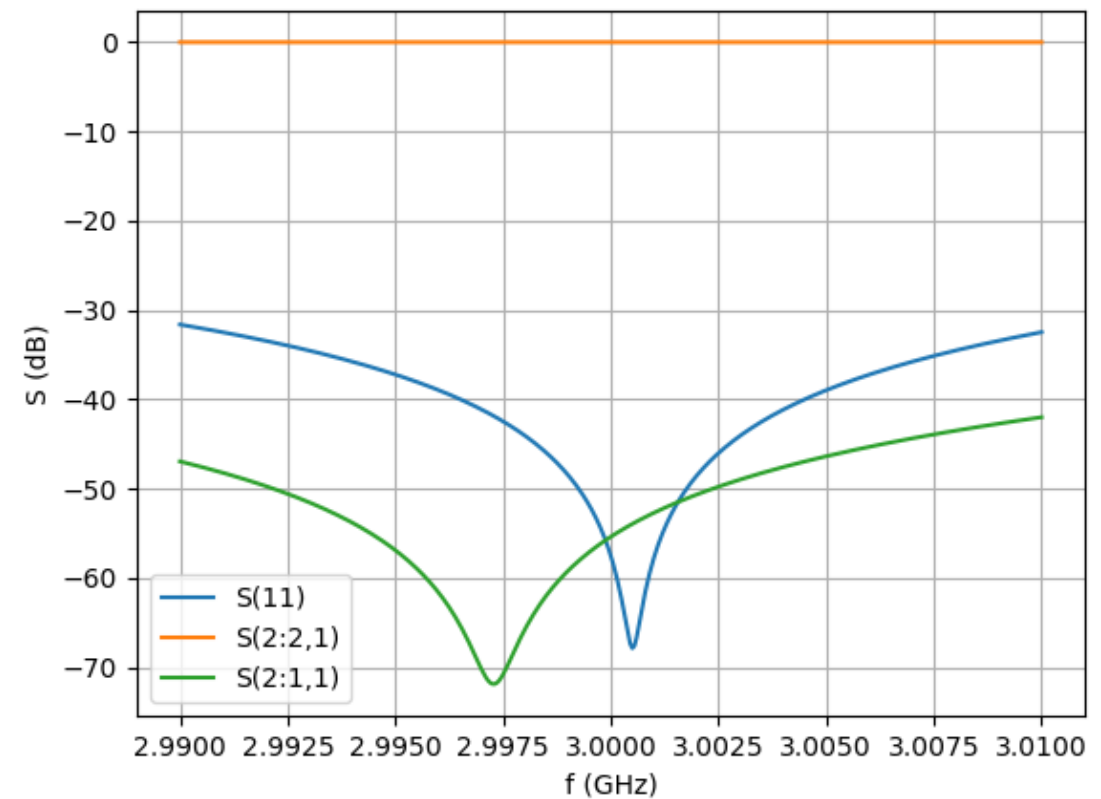




# Mode Launcher



- Minimize reflection:  $S(1,1)$
- Minimize transmission to  $TE_{11}$ :  $S(2:1,1)$
- Maximize transmission to  $TM_{01}$ :  $S(2:2,1)$



# Conclusions and next steps

- ❑ DAA results are promising but difficult to realize.
  - Paper published!!
- ❑ DDA prototype designed: good performance and easier fabrication

## **Next steps:**

- Multipactor mitigation
- Material testing and structure fabrication
- Mode launcher fabrication

# Conclusions and next

❑ DAA results are promising but difficult to

- Paper published!!

❑ DDA prototype designed: good performar

## Next steps:

- Multipactor mitigation
- Material testing and structure fabrica
- Mode launcher fabrication

**New year resolution: Write PhD thesis**

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Back up

# Non Linear effects

## Field Emission

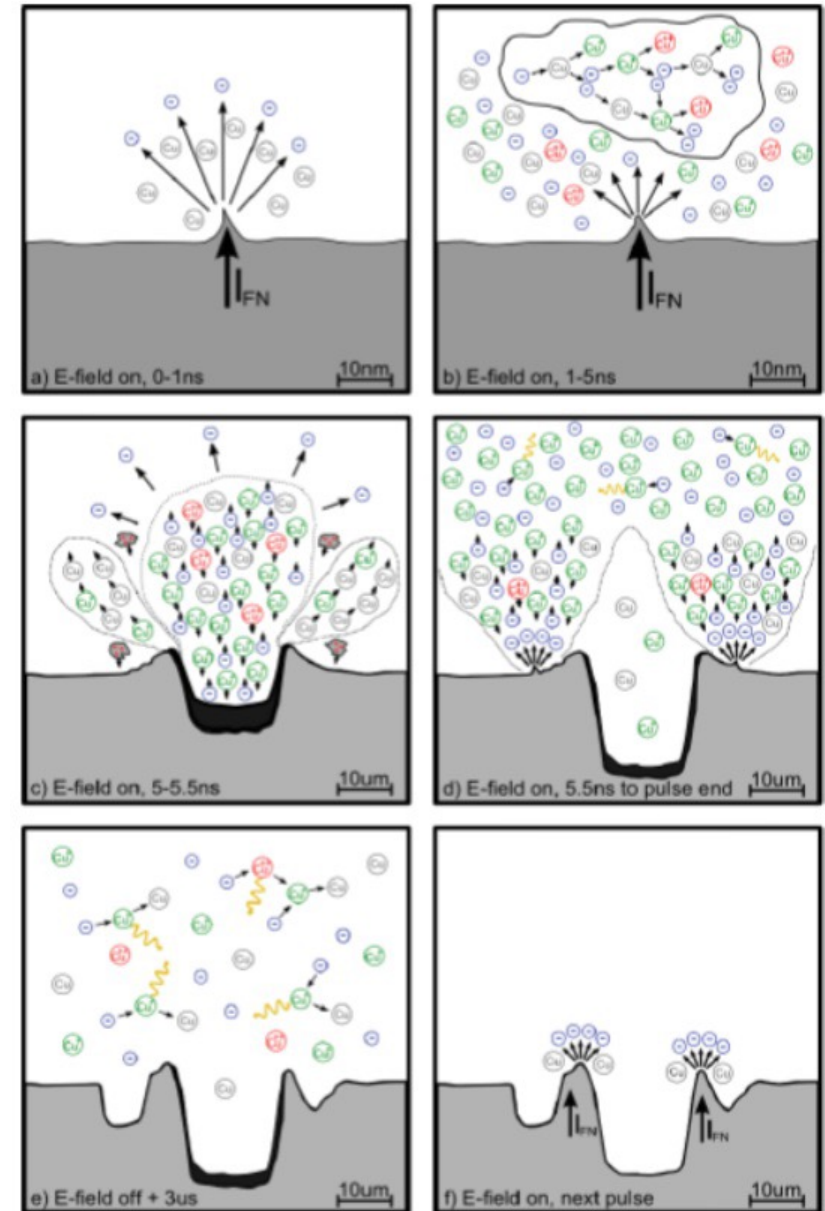
- ❑ Electrons are emitted by **tunneling** due to **High surface electric fields** following **Fowler-Nordheim equation**.

## RF Breakdown

- ❑ Electron currents burn protrusions **evaporating ion atoms**.
- ❑ Ions and electron cloud interact with electromagnetic fields producing **reflection effects**.

## Radiation

- ❑ Electrons interaction with walls translates into high radiation dose due to **bremsstrahlung photon emission**.

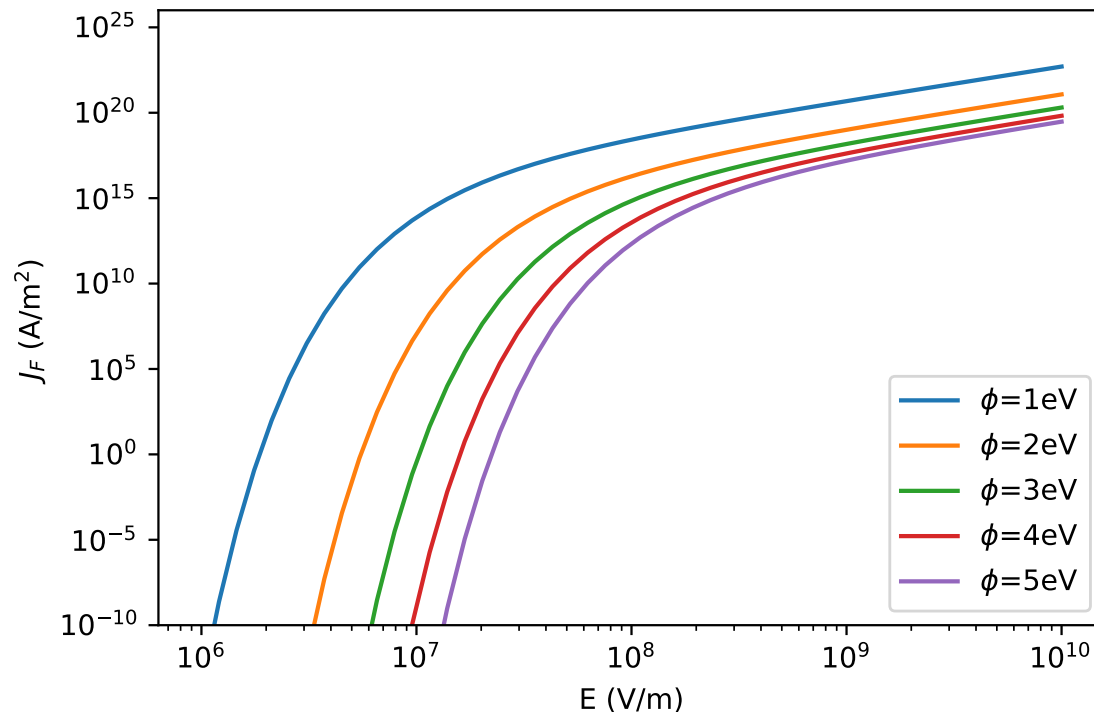


# Field emission

**Fowler-Nordheim** equation: Electrons are emitted through tunneling due to **high surface electric field**.

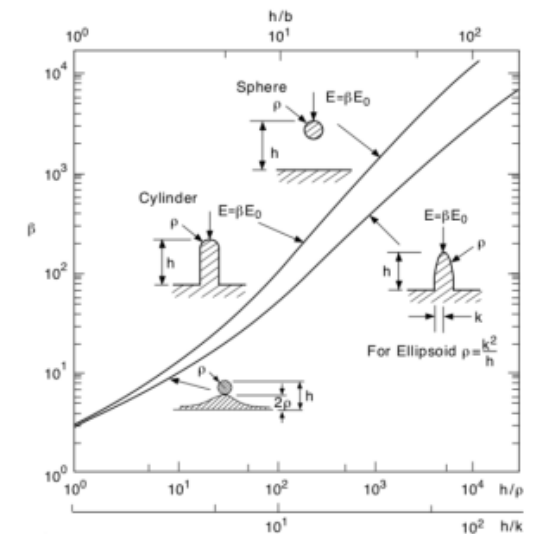
$$j_F = \frac{1.54 \times 10^{-6} \times 10^{4.52\phi^{-0.5}} E^2}{\phi} \exp \left[ -\frac{6.53 \times 10^9 \phi^{1.5}}{E} \right] \text{ A/m}^2$$

❑ Work function  $\phi$ : depends on material and geometry.



## Surface roughness:

Local enhancement factor  $\beta$  for different geometries of idealized metallic microprotusions:  $E_{id} = \beta \cdot E$



# High-Gradient limitation

## ❑ Surface magnetic field

Pulsed surface heating produced material fatigue -> cracks.

$$\Delta T \propto H_s^2 \sqrt{t_p},$$
$$\Delta T_{\max} = 50^\circ\text{C}$$

## ❑ Field emission due to surface electric field

- RF breakdowns; Electron emission initiates vacuum arcs. The exact mechanism is still unclear.
- Breakdown rate (BD/pulse.m) -> Operation efficiency;
- Local plasma triggered by field emission -> Erosion of surface;
- Dark current capture -> Efficiency reduction, detector backgrounds.

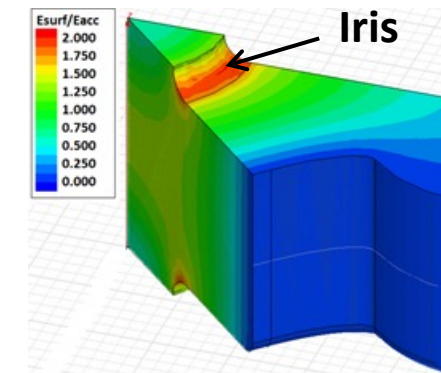
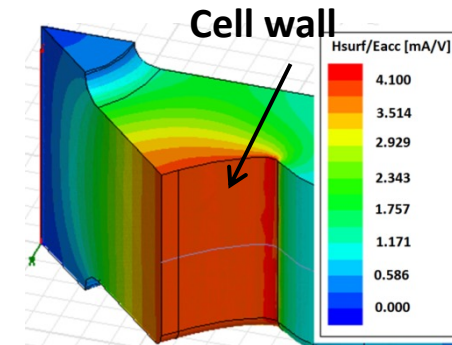
$$E_s = 200 \frac{\text{MV}}{\text{m}}$$

## ❑ RF power flow

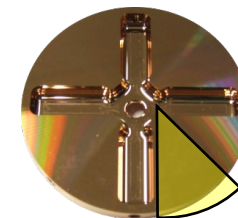
RF power flow and/or iris aperture has a strong impact on achievable  $E_{acc}$  and on surface erosion.

Modified Poynting vector:

$$S_c = |Re(\vec{S})| + \frac{1}{6}|Im(\vec{S})|$$
$$5 \text{ MW/mm}^2$$



[W. Wuensch et al. Phys. Rev. ST Accel. Beams **12**, 102001 (2009)]



# RF breakdown criteria

## ❑ Kilpatrick's Criterion.

$$f = 1.64[\text{MHz}](E_s[\text{MV/m}])^2 \exp\left(\frac{-8.5}{E_s[\text{MV/m}]}\right)$$

- Underestimation

## ❑ $P/C$

$$P = \frac{v_g a Q}{\omega R} E_{acc}^2 \quad C: \text{Circumference of iris}$$

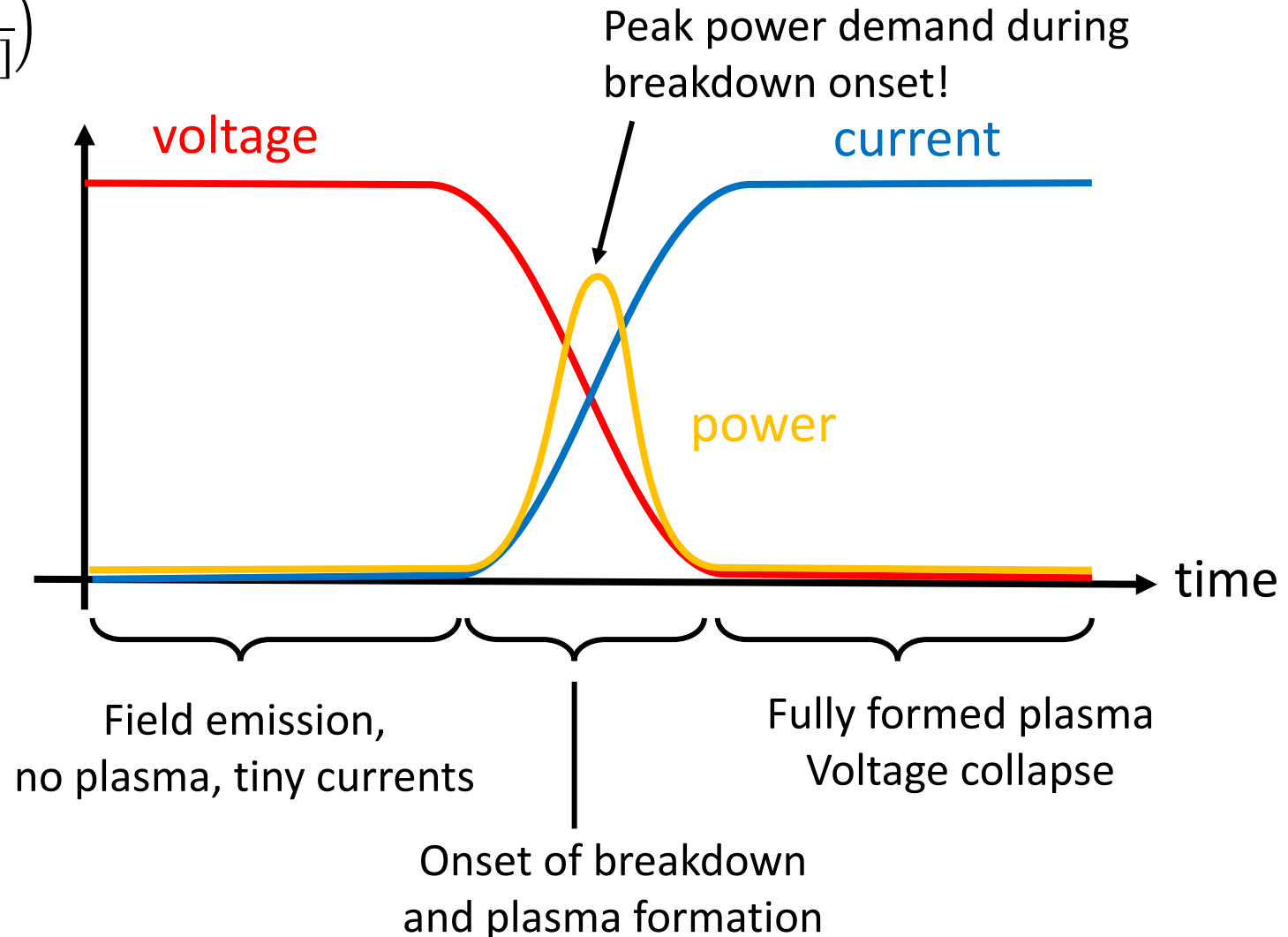
- Only valid for travelling wave

## ❑ Modified Poynting Vector: $S_c < 5 \text{ MW/mm}^2$

$$S_c = \text{Re}(\mathbf{S}) + \frac{1}{6} \text{Im}(\mathbf{S})$$

- Exceptions found (Crab cavity)

## ❑ Local Power Coupling

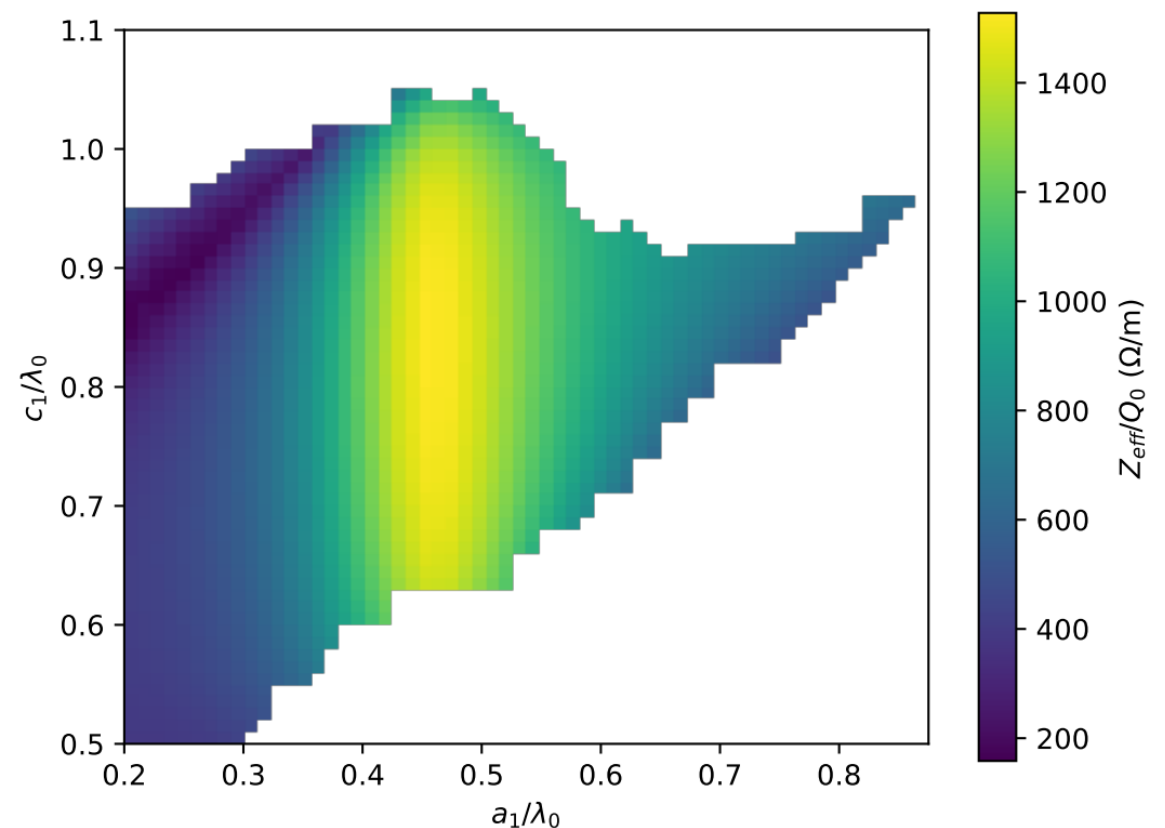
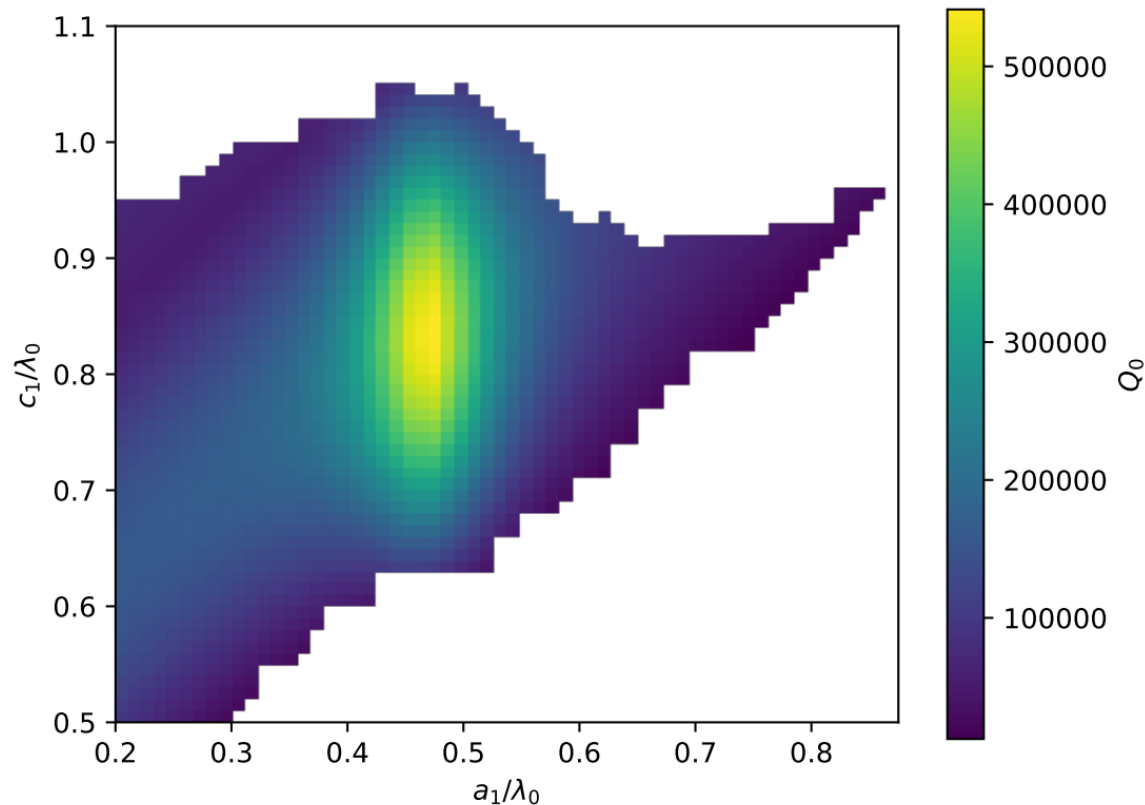
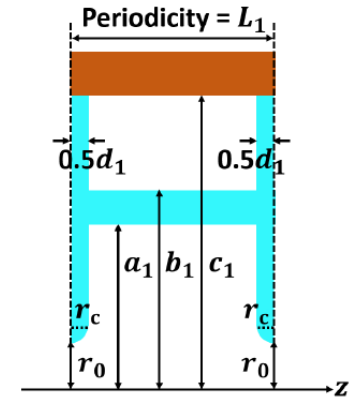


# DAA cavity single cell design

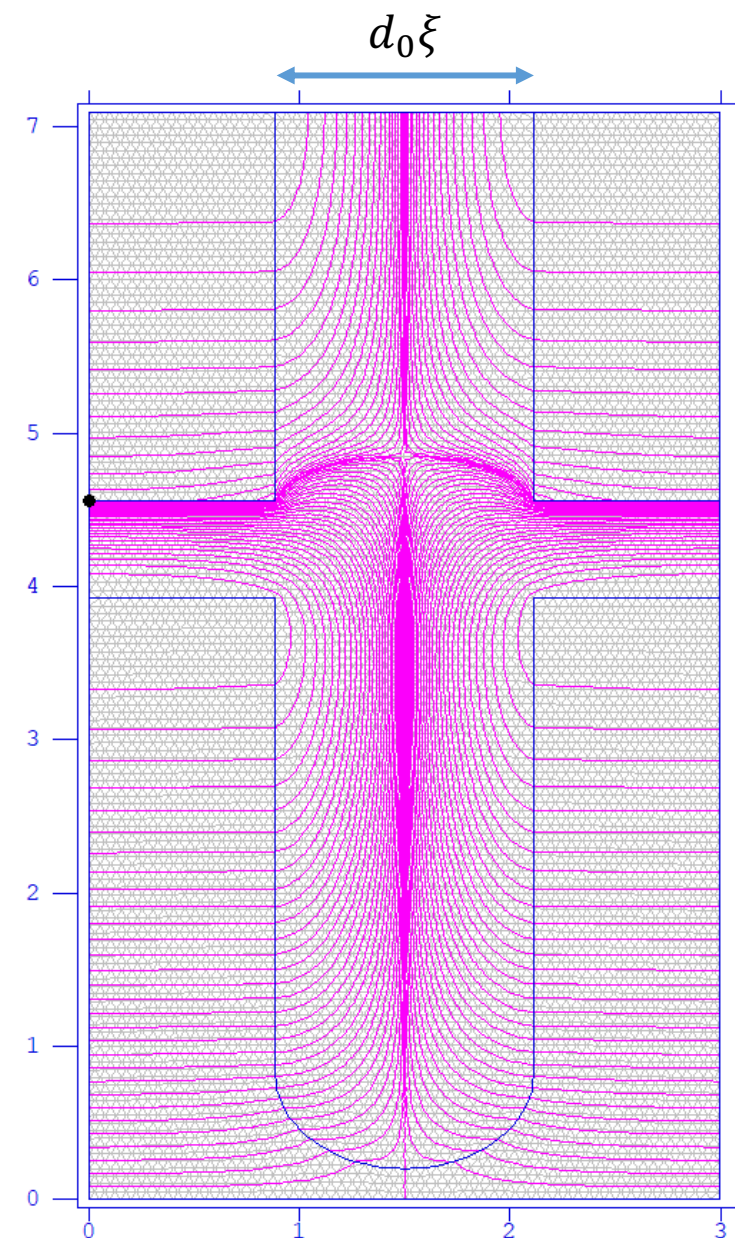
Resonant frequency for the mode depends on the combination of  $a_1, b_1, c_1$ :

- ❑ Scan for  $a_1, c_1$  and we look for the value of  $b_1$  that makes  $f = (3000 \pm 2)$  MHz.
- ❑ Look for the values of  $a_1, b_1, c_1$  that maximizes  $Z_{eff}, Q_0$

Example for ideal material:  $\epsilon_r = 16.66$ ,  $\tan \delta = 0$  and  $\beta = 0.6$



# DAA cavity single cell iris optimization



$$\epsilon_r = 16.66, \beta = 0.6$$

Scan in iris thickness:  $d_0 = \lambda_0 / (4\sqrt{\epsilon_r})$

Iris thickness =  $d_0\xi$

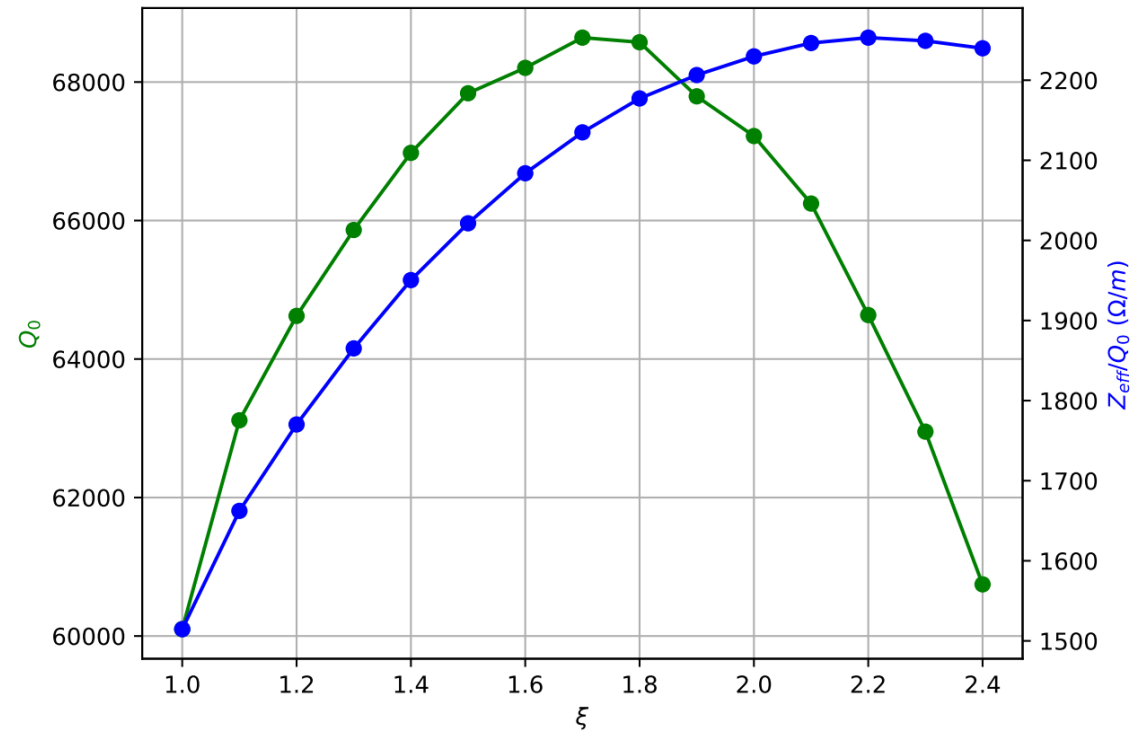


TABLE I  
LIST OF DIELECTRICS STUDIED IN THE OPTIMIZATION

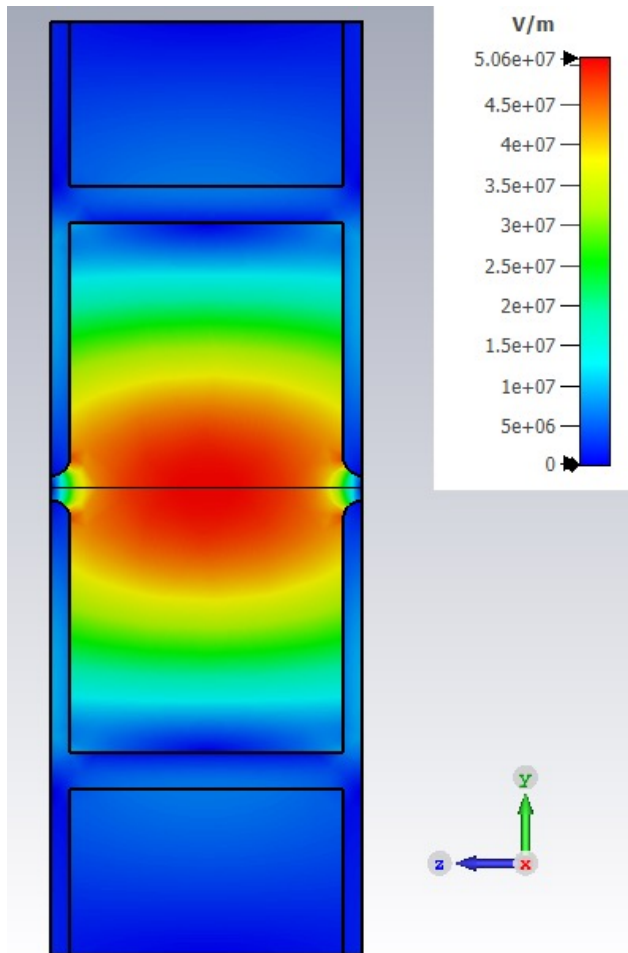
Material	Acronym	$\epsilon_r$	$\tan \delta$
CVD Diamond	Diamond	5.7	$10^{-4}$
MgO	D9	9.64	$6 \times 10^{-6}$
MgTiO <sub>3</sub>	D16	16.66	$3.43 \times 10^{-5}$
BaTiO <sub>x</sub>	D50	50.14	$8 \times 10^{-5}$

$$\beta = \{0.4, 0.5, \dots, 1\}$$

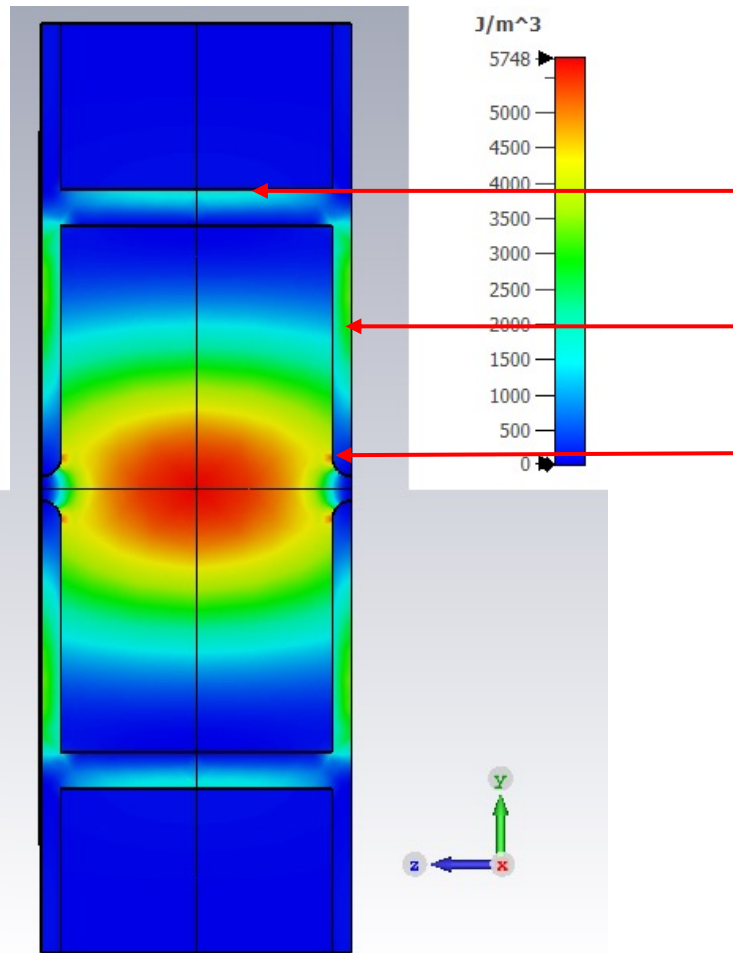


# DAA cavity single cell solution

Electric field



Electric Energy



$$D = \epsilon E$$

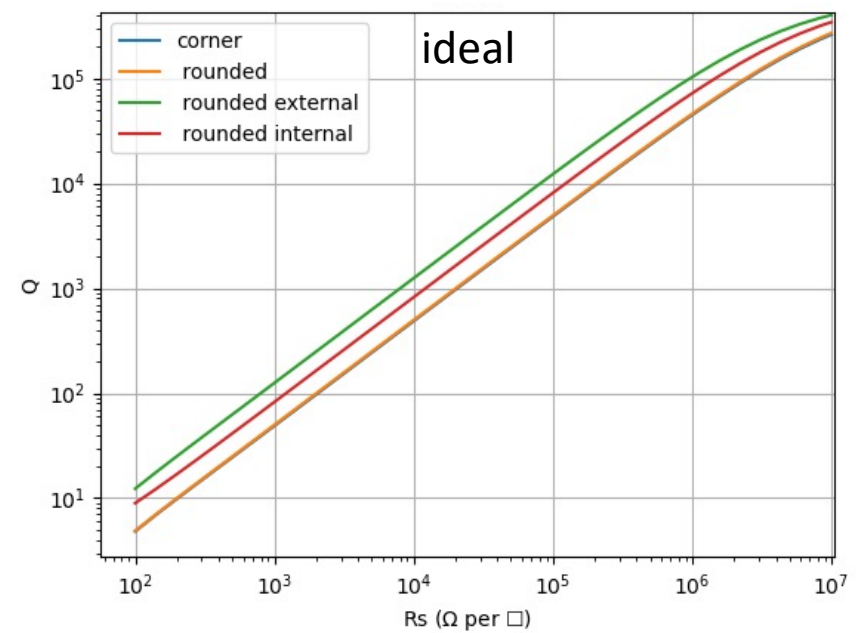
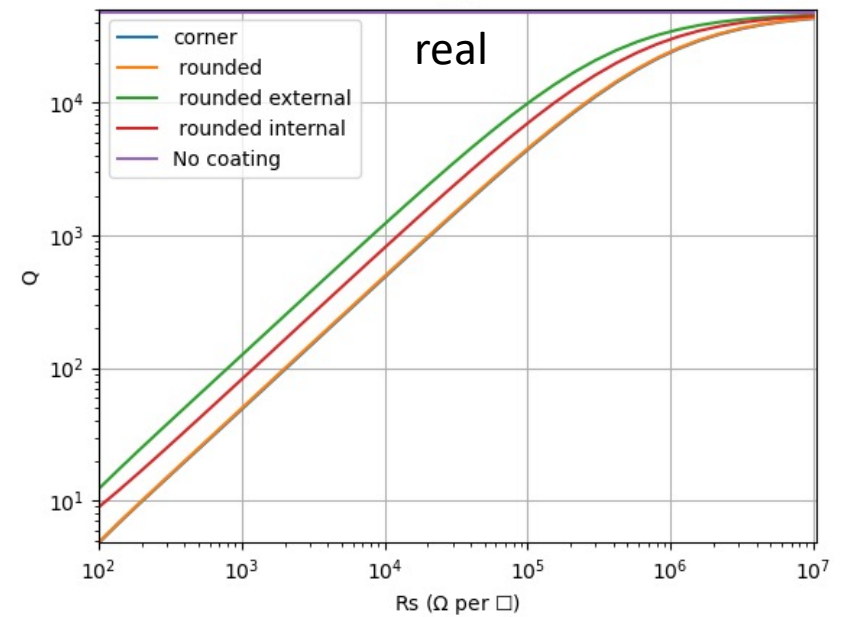
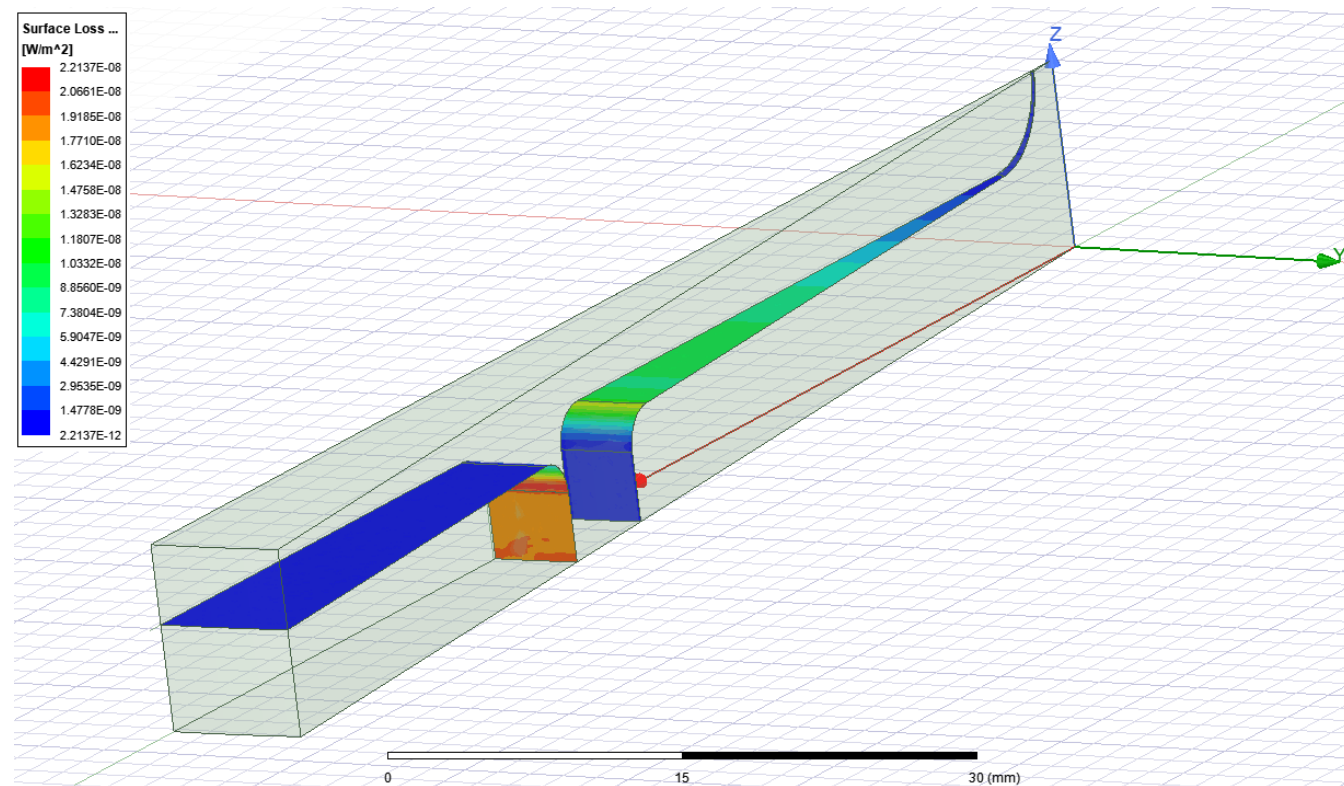
$$E_{\parallel,1} = E_{\parallel,2}$$

$$D_{\perp,1} = D_{\perp,2}$$

- 1<sup>st</sup>: Parallel boundary  $\left\{ \begin{array}{l} E \text{ is constant} \\ \text{High } D \text{ inside dielectric} \end{array} \right.$
- 2<sup>nd</sup> :  $D$  is conserved along the dielectric
- 3<sup>rd</sup> : Perpendicular boundary  $\left\{ \begin{array}{l} D \text{ is constant} \\ \text{High } E \text{ in vacuum} \end{array} \right.$

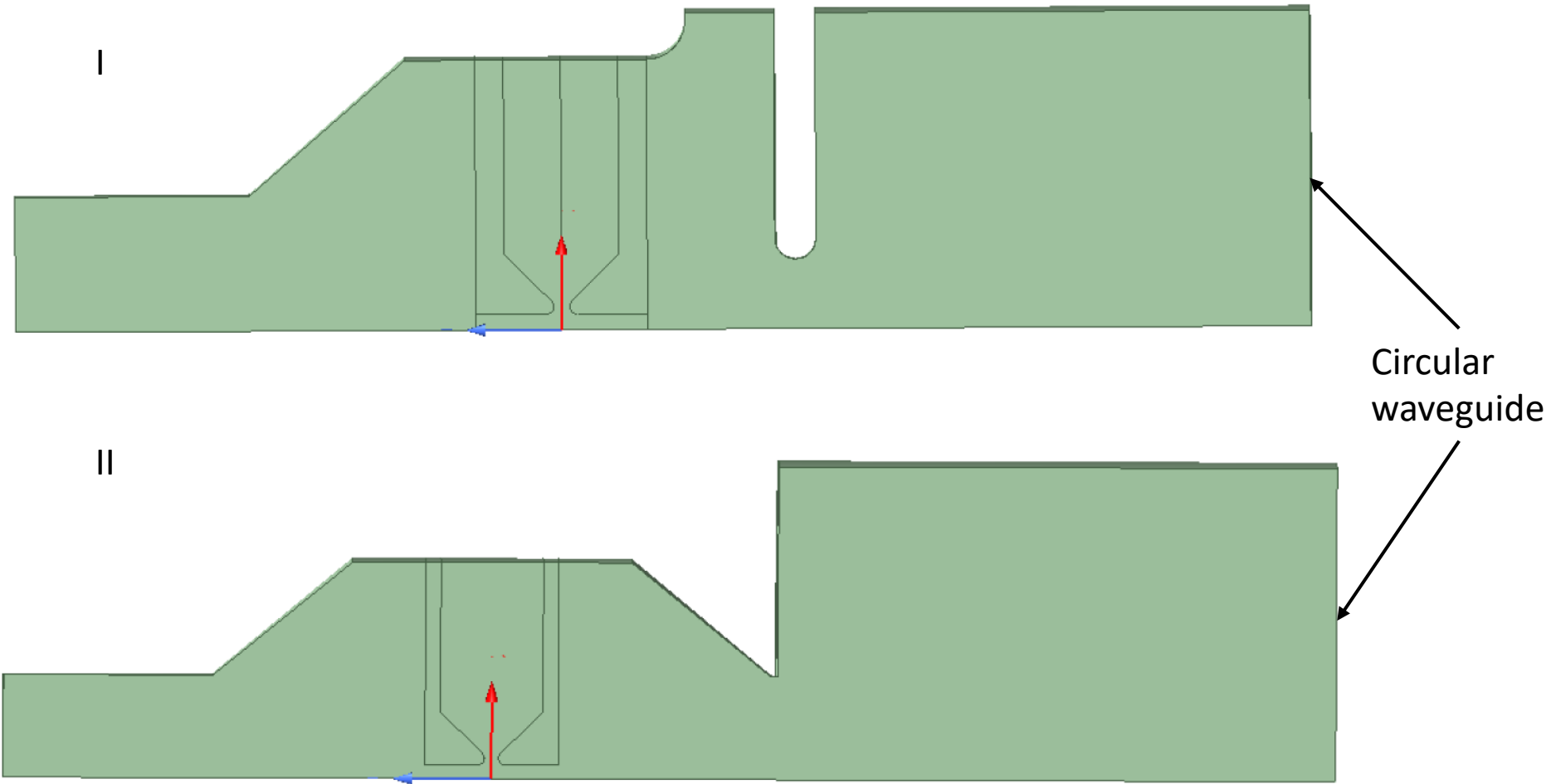


# Coating losses

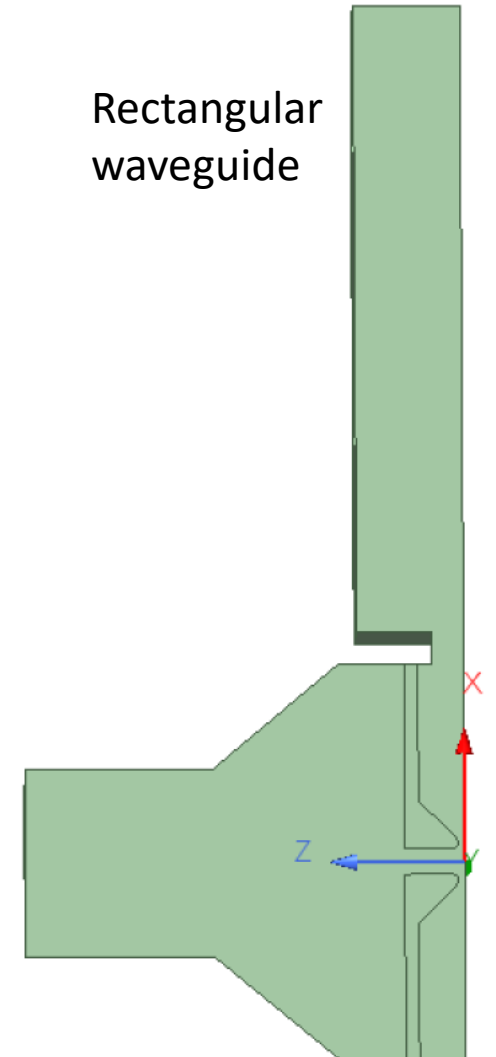


# DDA prototype

**Electric coupling**



**Magnetic coupling**



# Dielectric Disk Loaded Accelerating (DDA) Cavity

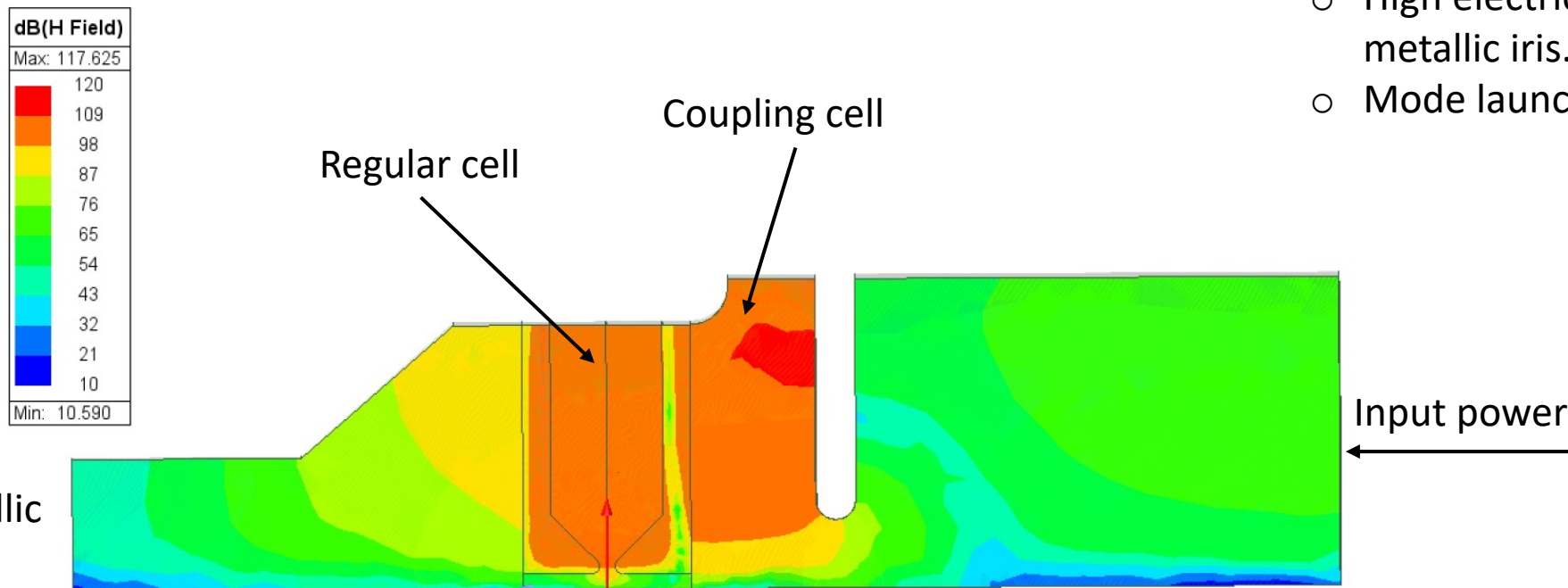
## Electric coupling I

### Pros:

- Coupling can be adjusted easily
- Low coupling to other modes

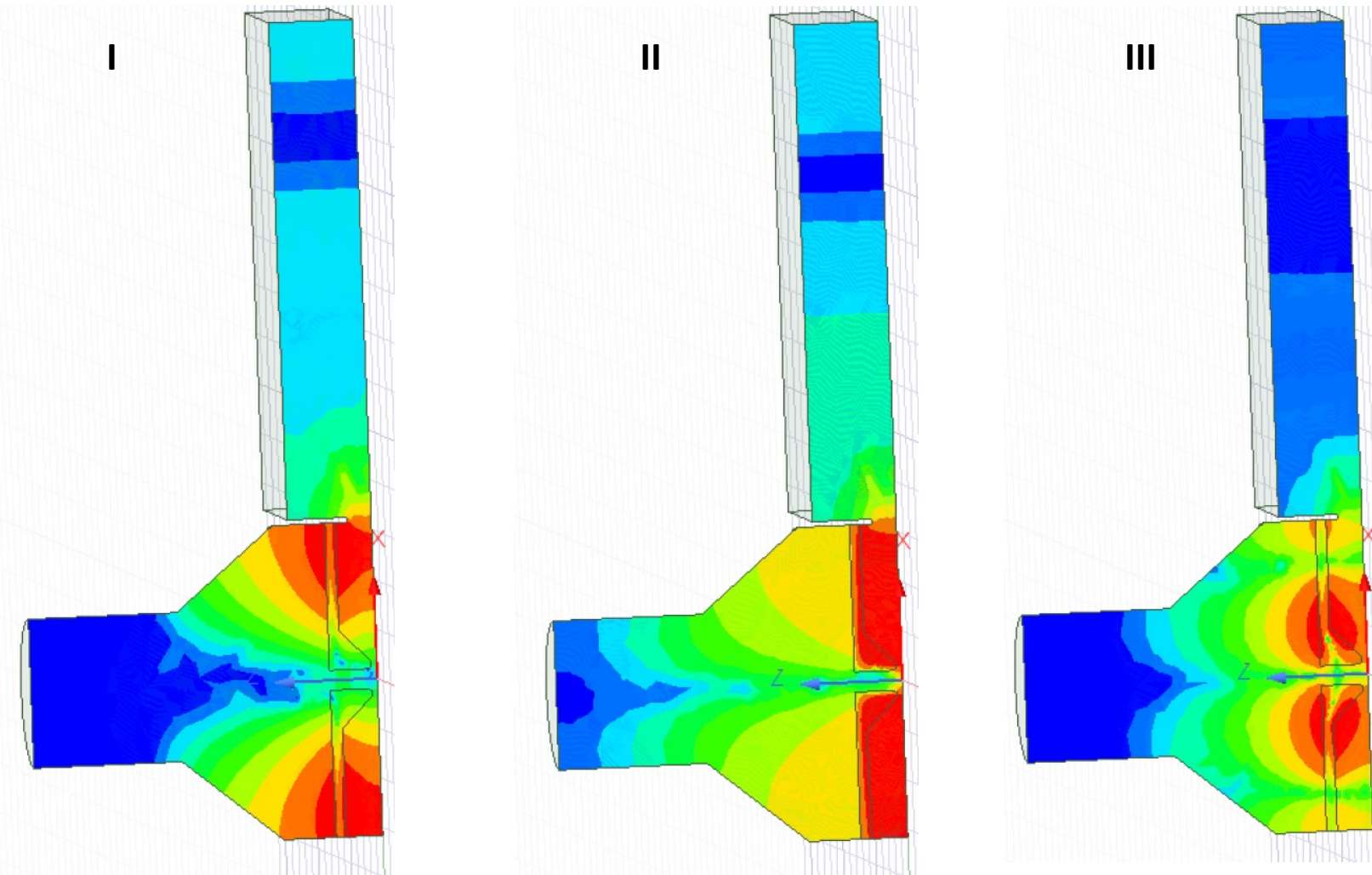
### Cons:

- High magnetic field in coupling cavity: lower  $Q$
- High electric field on coupling metallic iris.
- Mode launcher needed.



# Dielectric Disk Loaded Accelerating (DDA) Cavity

## Magnetic coupling



### Pros:

- Low magnetic field in coupling cavity:
- Low electric field on coupling metallic iris.
- No need for mode launcher.

### Cons:

- Low coupling to mode
- Similar coupling to other modes

# Dielectric Disk Loaded Accelerating (DDA) Cavity

D50,  $\beta = 0.4$ ,  $\epsilon_r = 50.14$ ,  $\tan \delta = 8 \times 10^{-5}$ ,  $\xi = 1.5$ ,  $gap = 0.2 \text{ cm}$ ,  $\alpha = 45^\circ$ ,  $r = 0.1 \text{ cm}$

Eigenmode solver

Parameter	value
$Q_0$ (regular cell)	21503
$Q_{ext}$	22070
$Q_l$	11380
$Q_0$ (total)	23494

$$Q_l = \frac{f_{res}}{BW} = 11197$$

Electric coupling II

