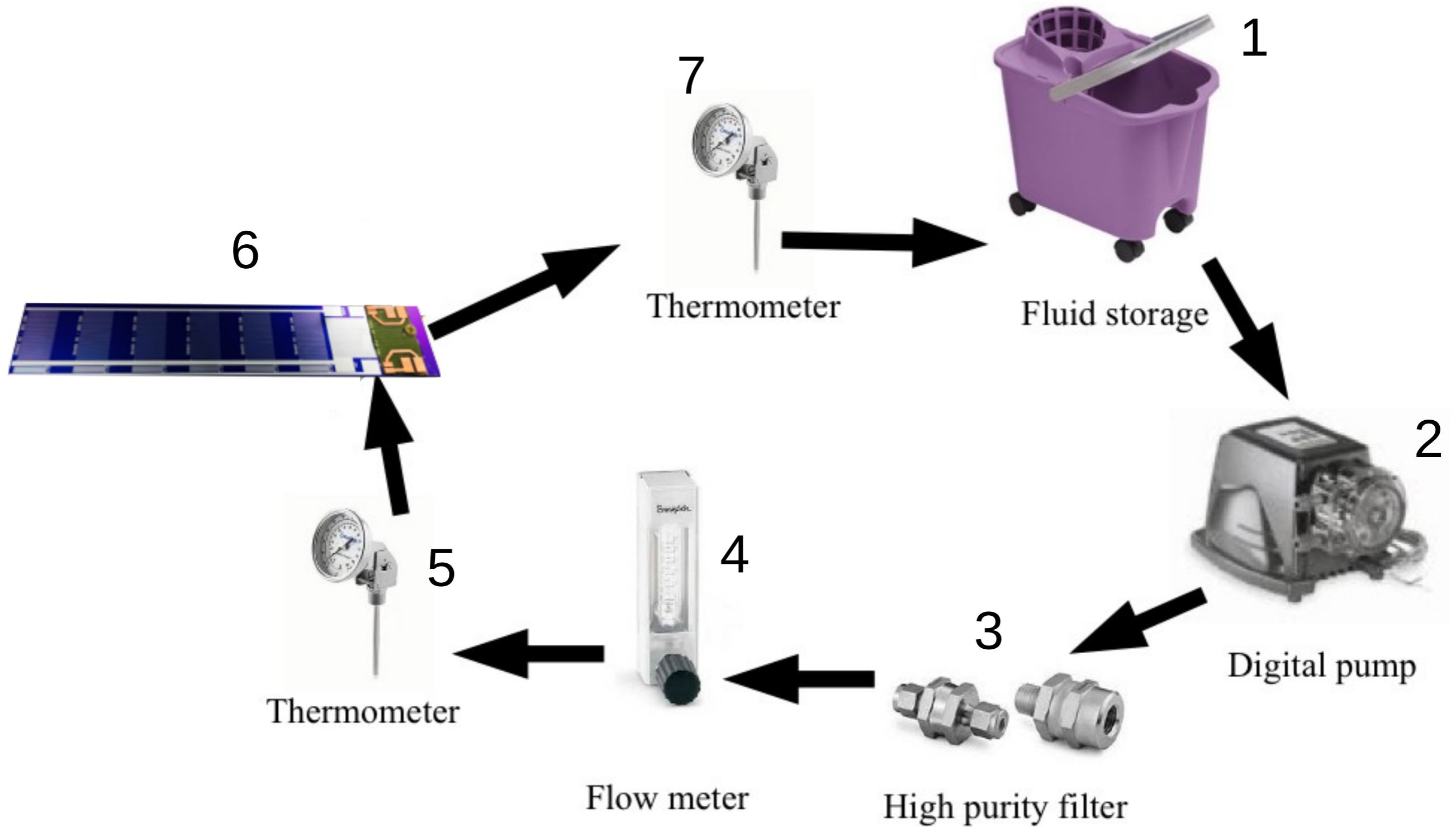
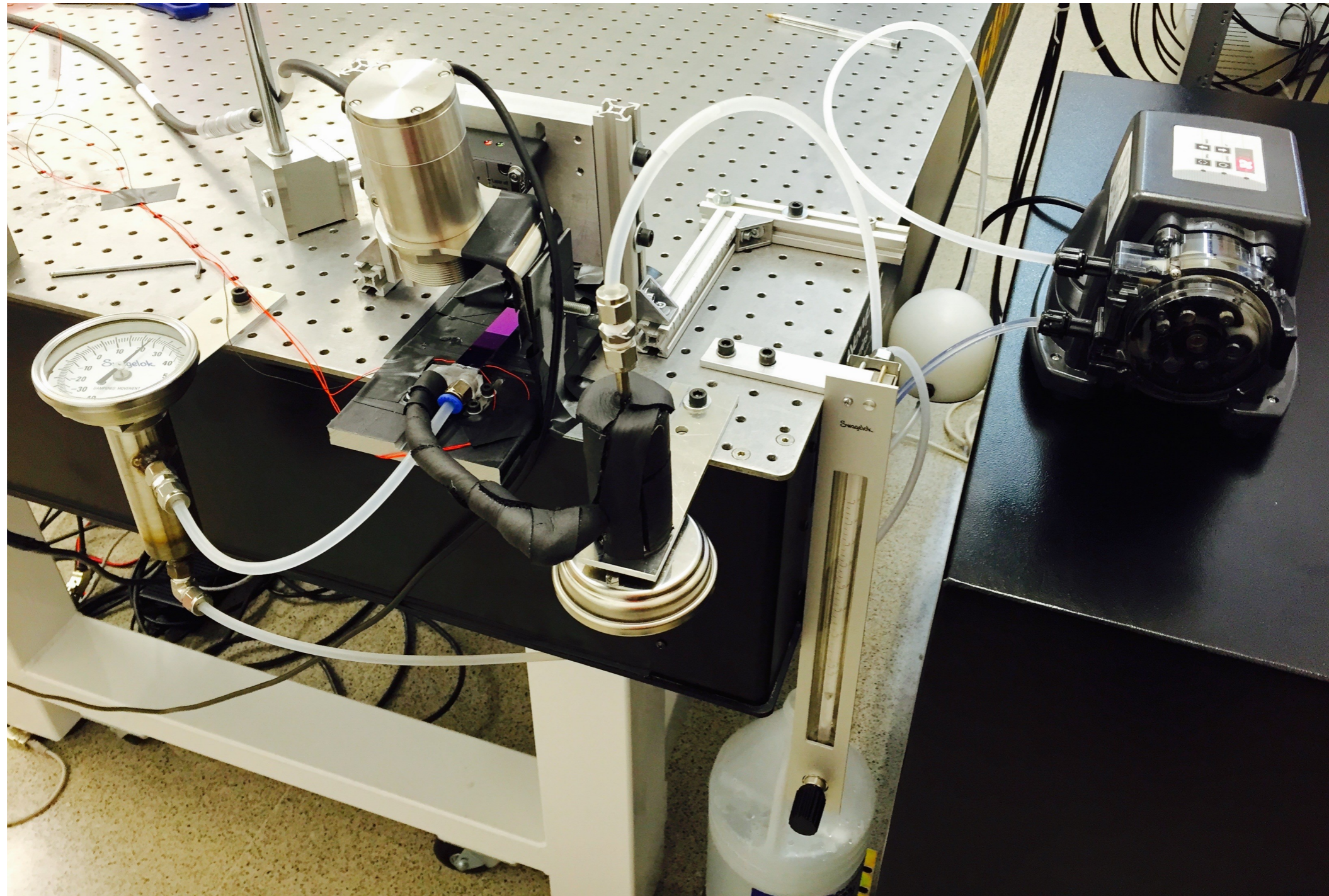


MC Cooling Update from IFIC

Experimental setup



Experimental setup



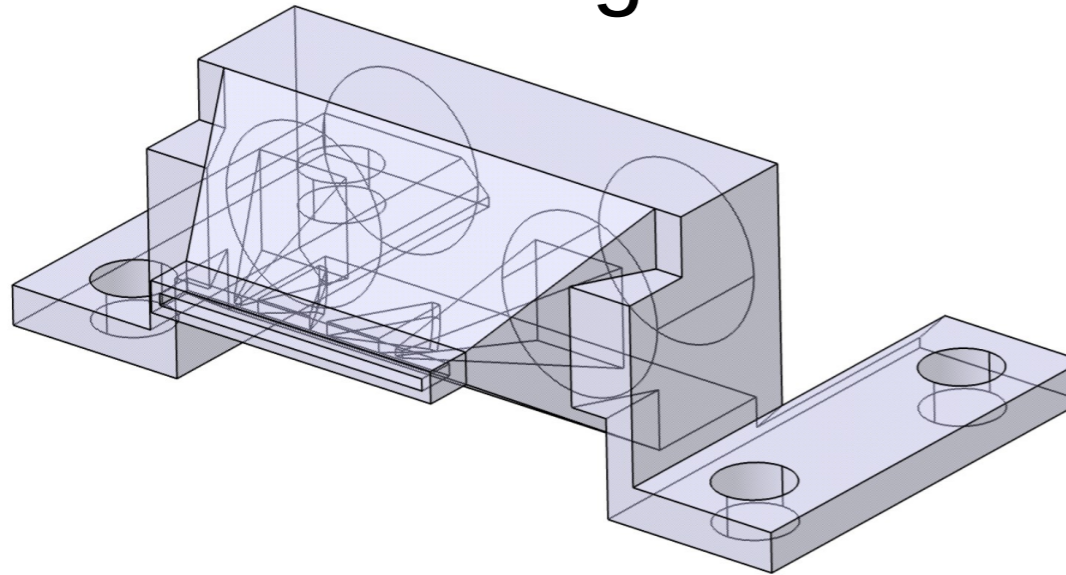
3D-printer technology

Built by 3D-printer (stereolithography technology):

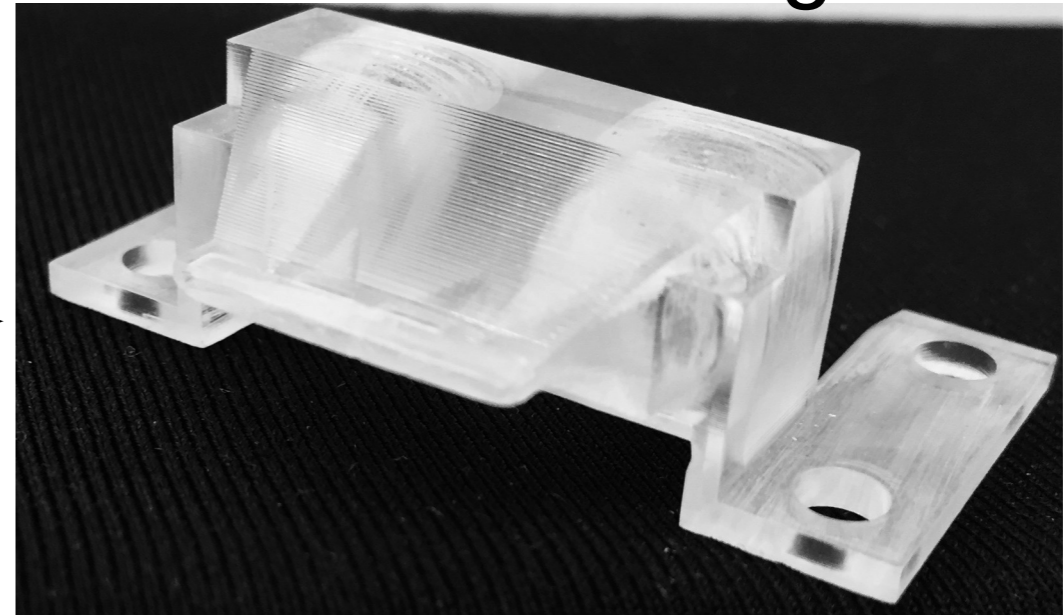
- 15 μm precision
- 300 μm per layer
- Very complex geometries
- Material: X0=350mm
- Joint: 3D Part glued to MC silicon module
- Cheap and fast manufacture (not the 3D printer)
- Good performance below 70°C

3D-printed adaptor PREVIOUS design

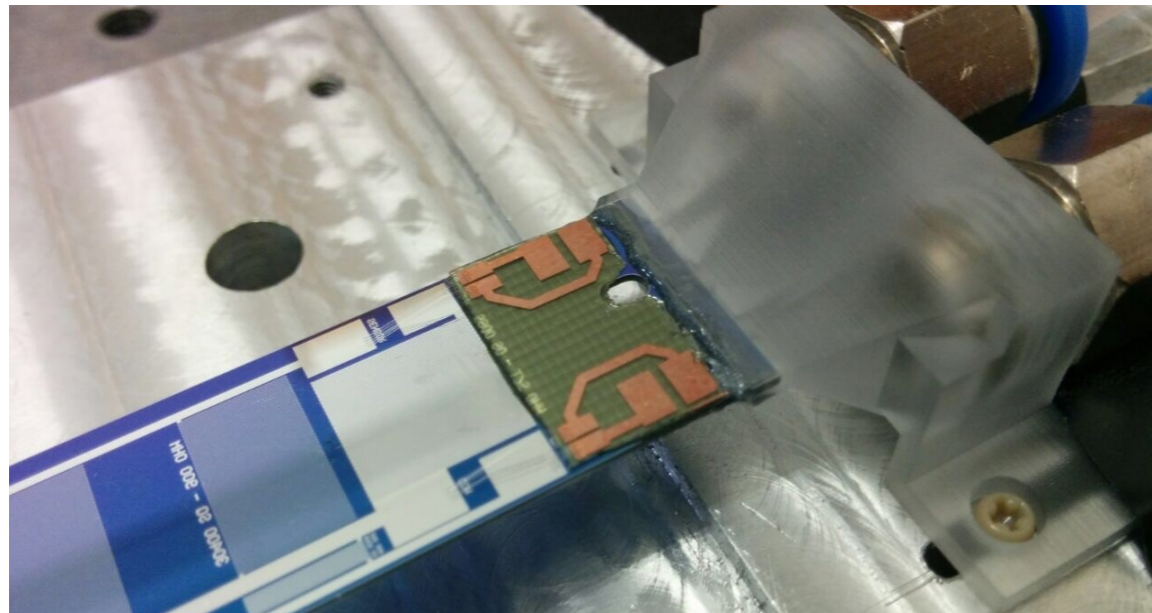
Design



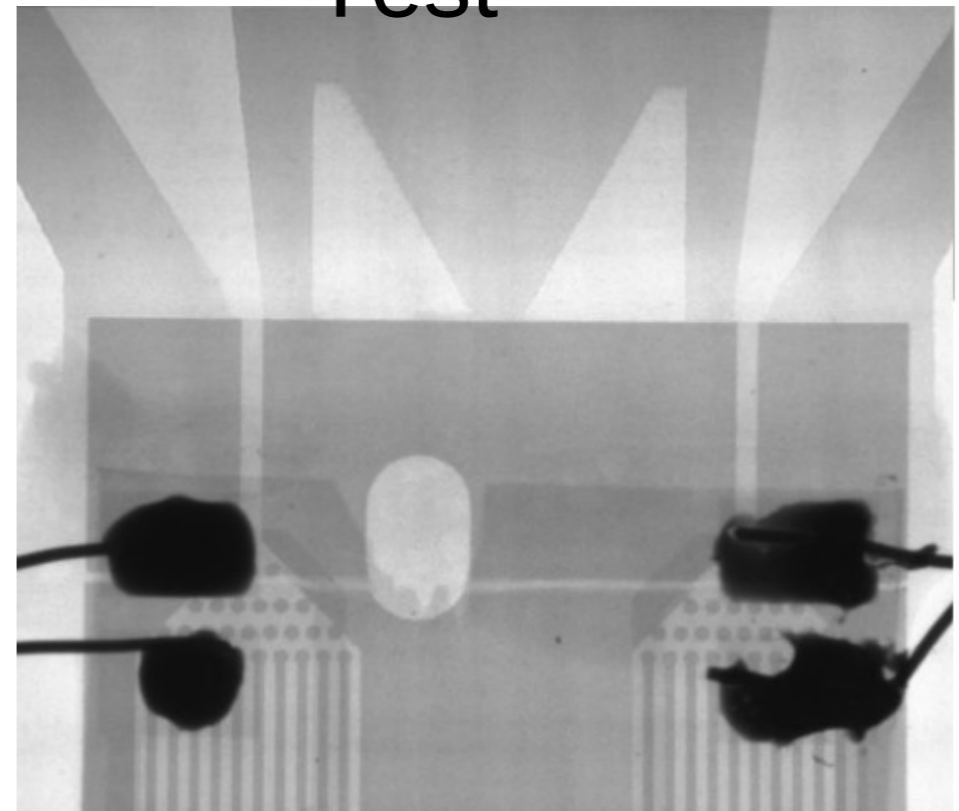
3D-Printing



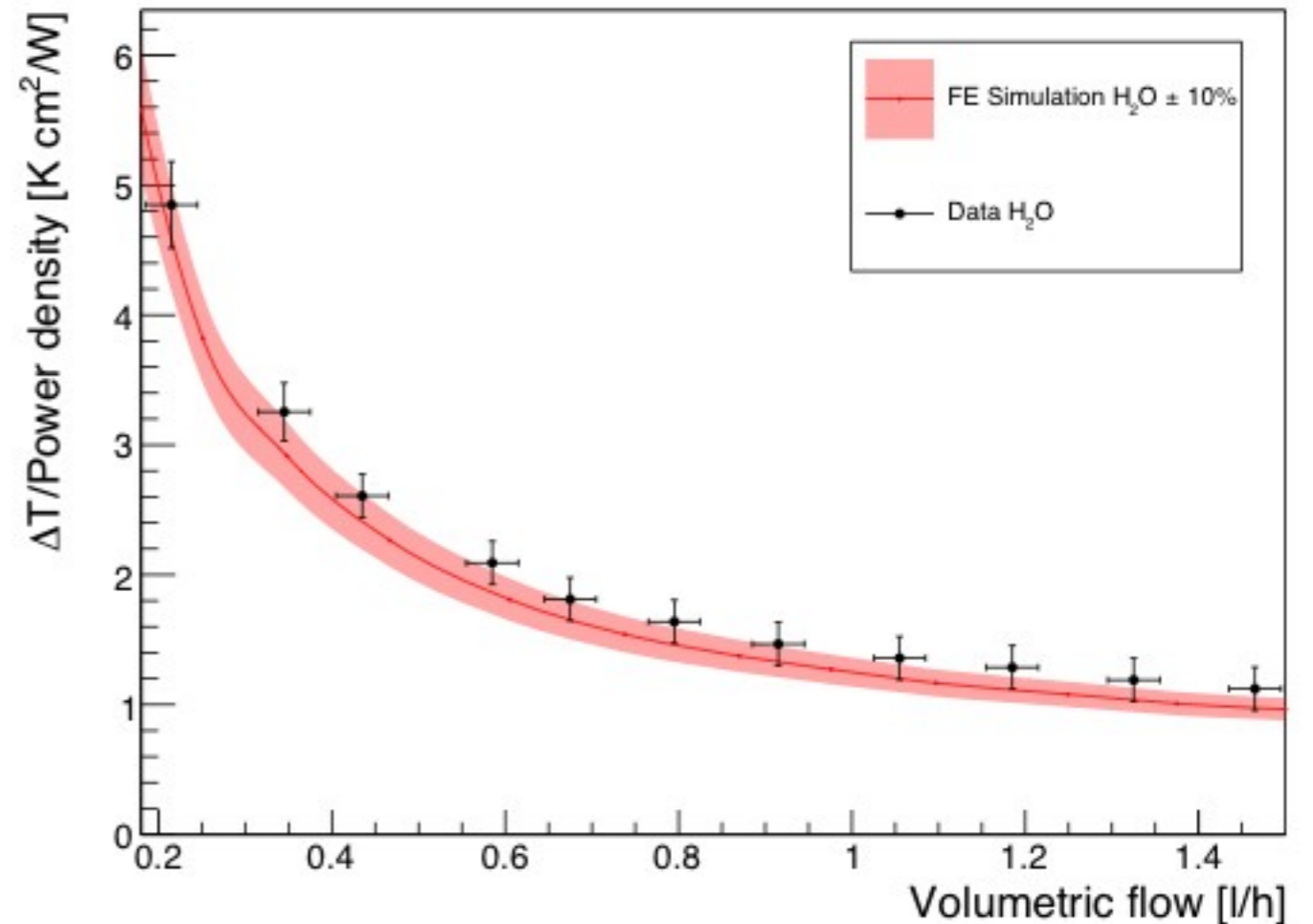
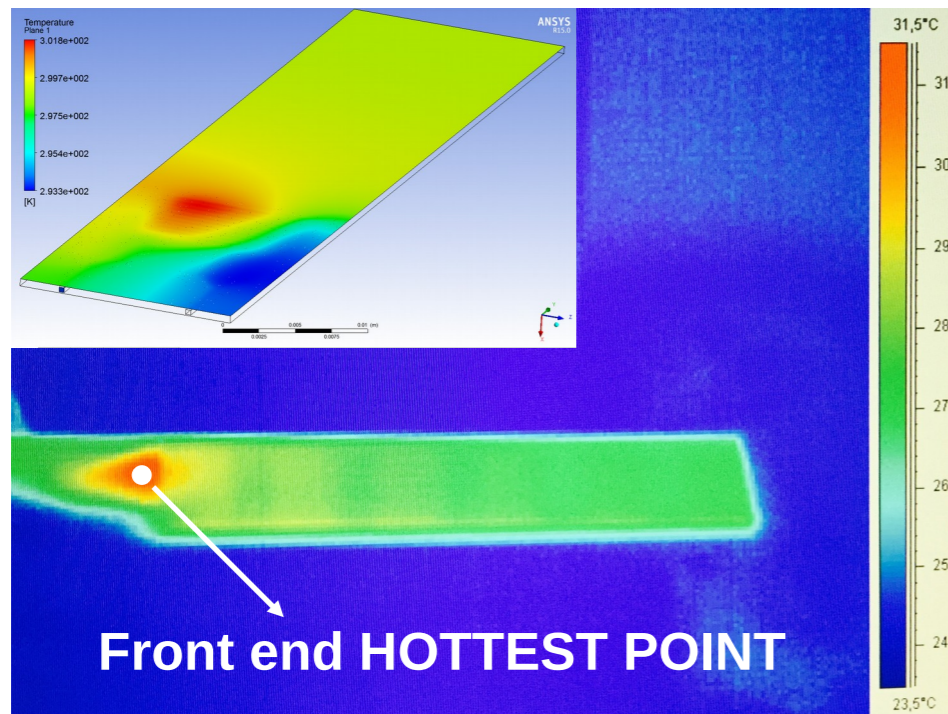
Gluing



Test



Thermal measurements: MCC

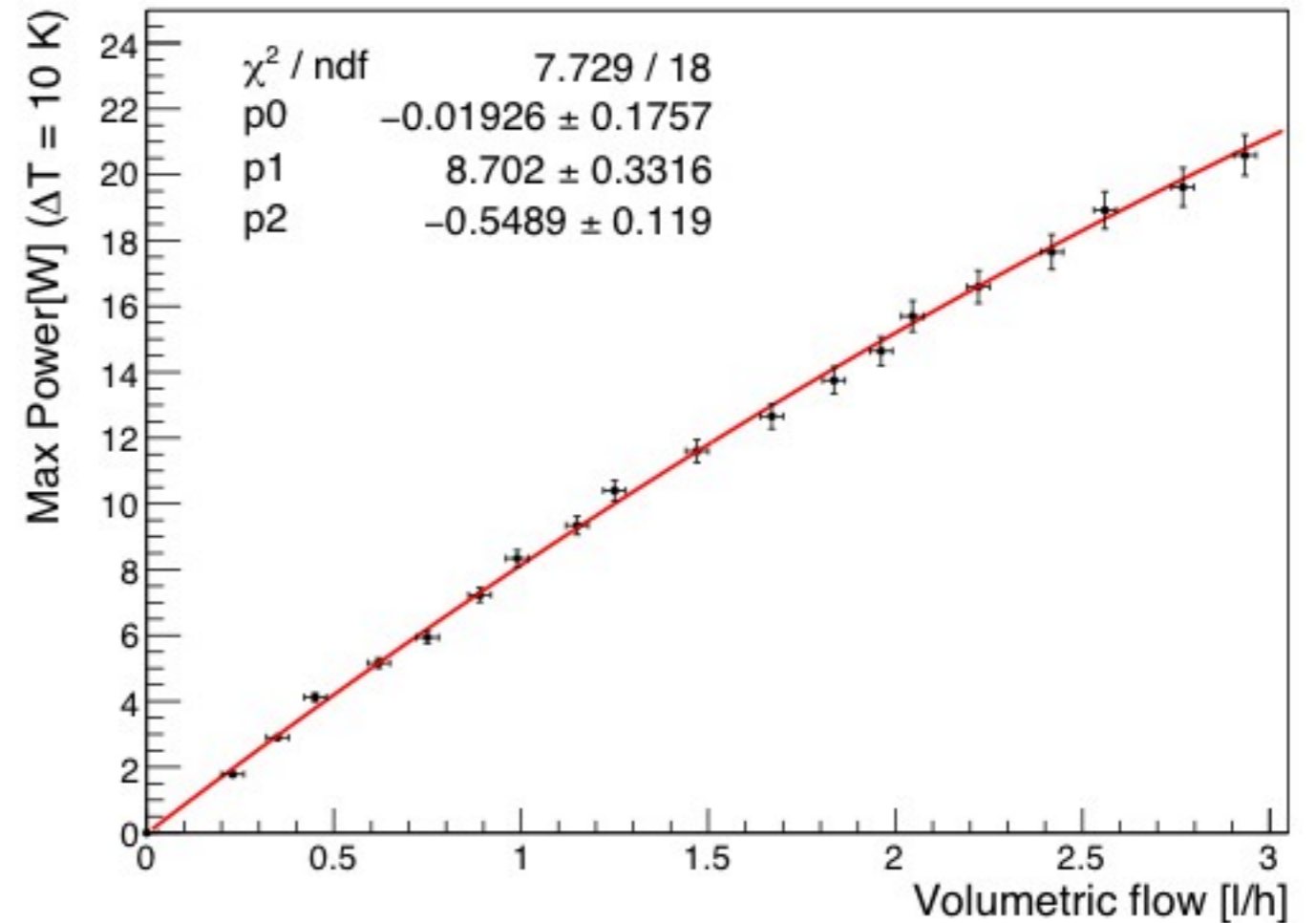
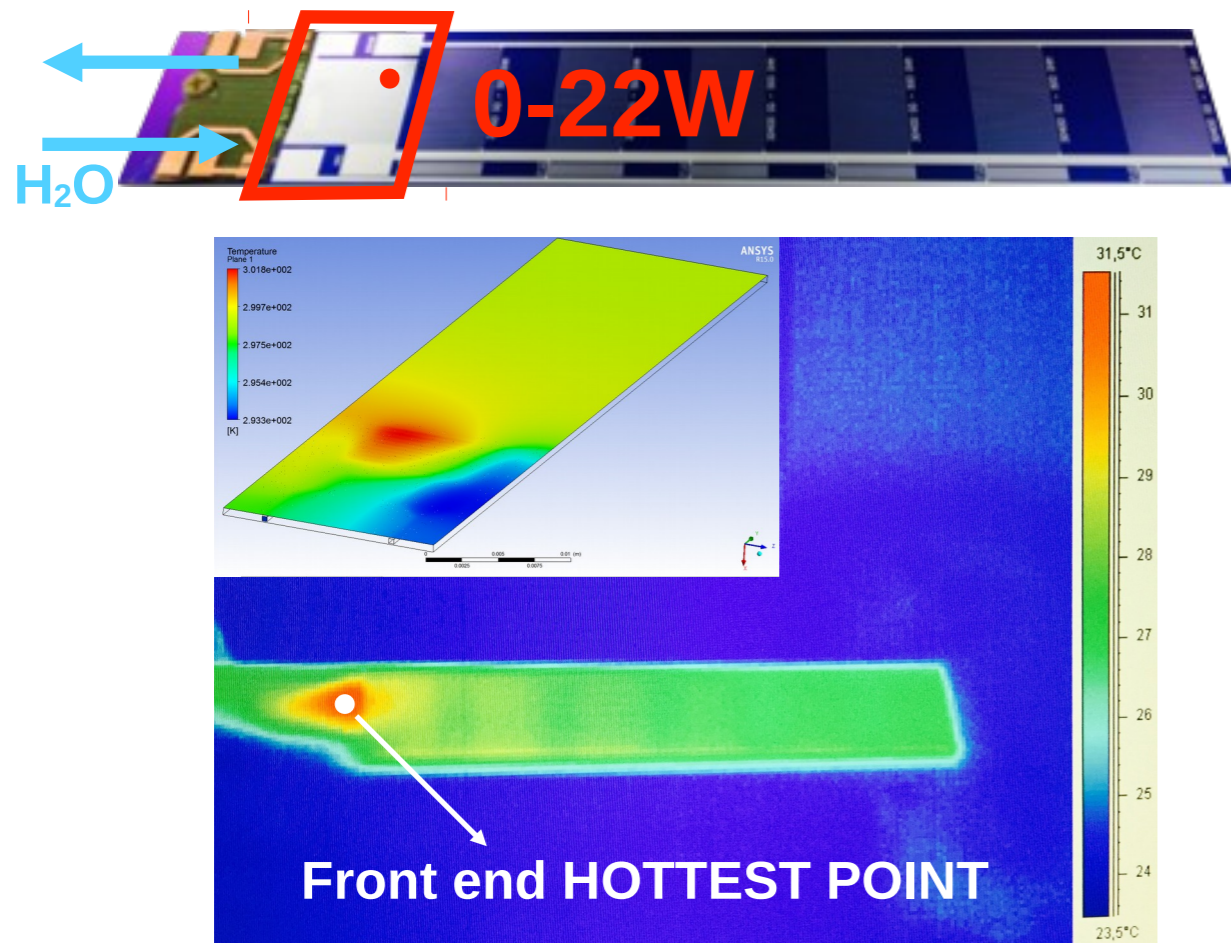


- Fluid: H₂O
- **With flows (~1l/h) and low pressure drop (<1bar) are good enough**
- **Good agreement with the FE simulation inside an error area of 10%**

Measurement data errors

- P ±1% W
- T ± 1 °C
- ΔT/Power density ± 0,14 °C/W
- flow ± 0,03 l/h

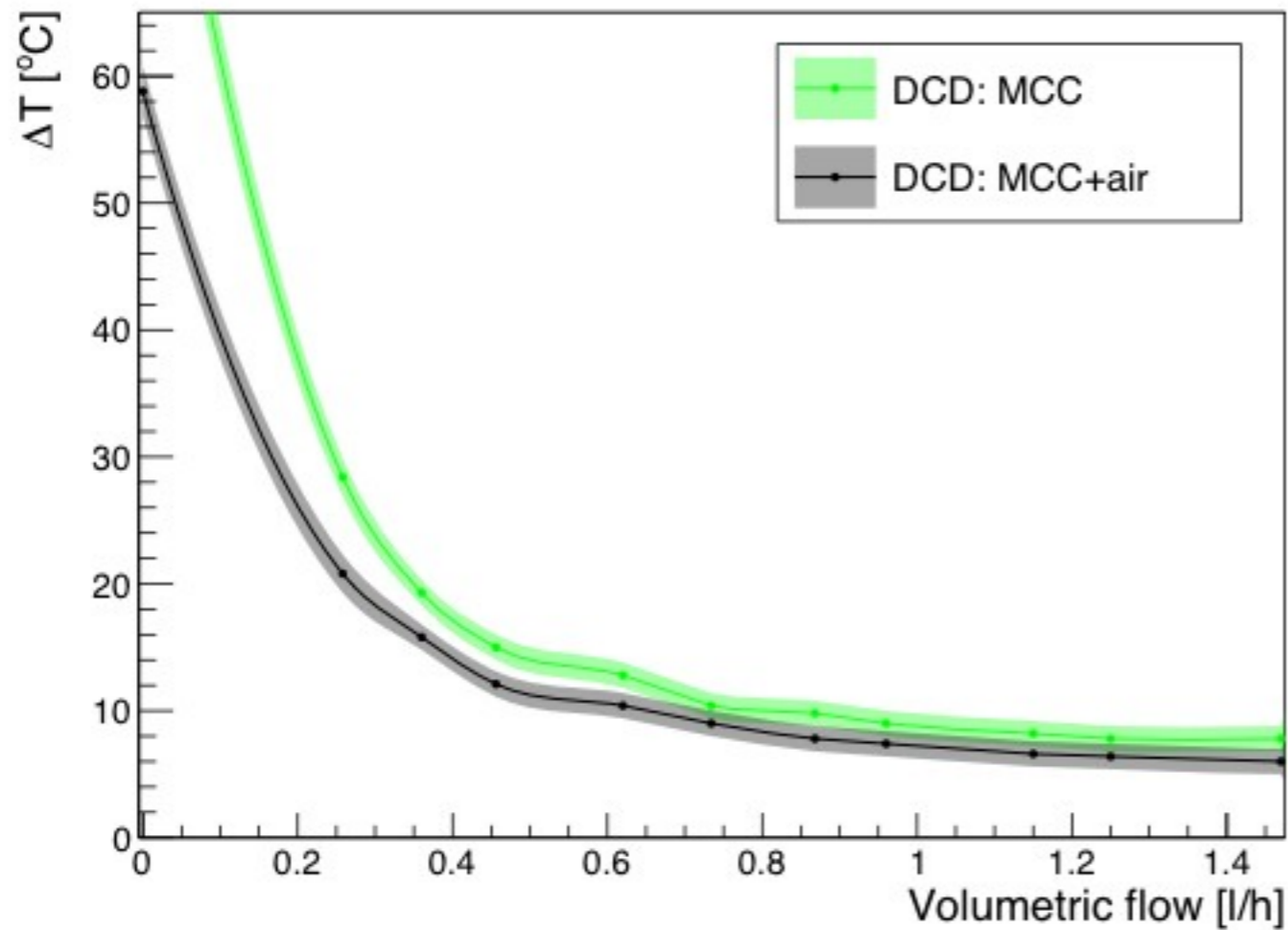
Thermal measurements: Maximum Power vs Volumetric flow



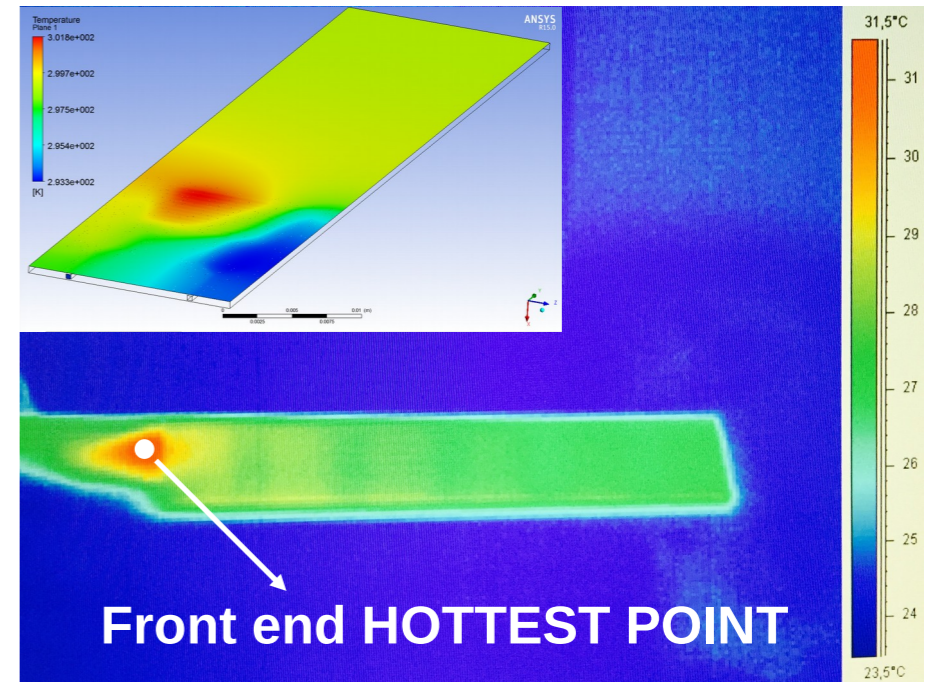
Maximum power supported for a ΔT of 10 °C as a function of the volumetric flow

- **Temperature stable** even with power density of **25 W/cm²**
- **Power vs vol. flow** at max. pump power (~ 3 l/h)
- **Low pressure** needed: 0.2 - 1.5 bar

Thermal measurements: MCC+air

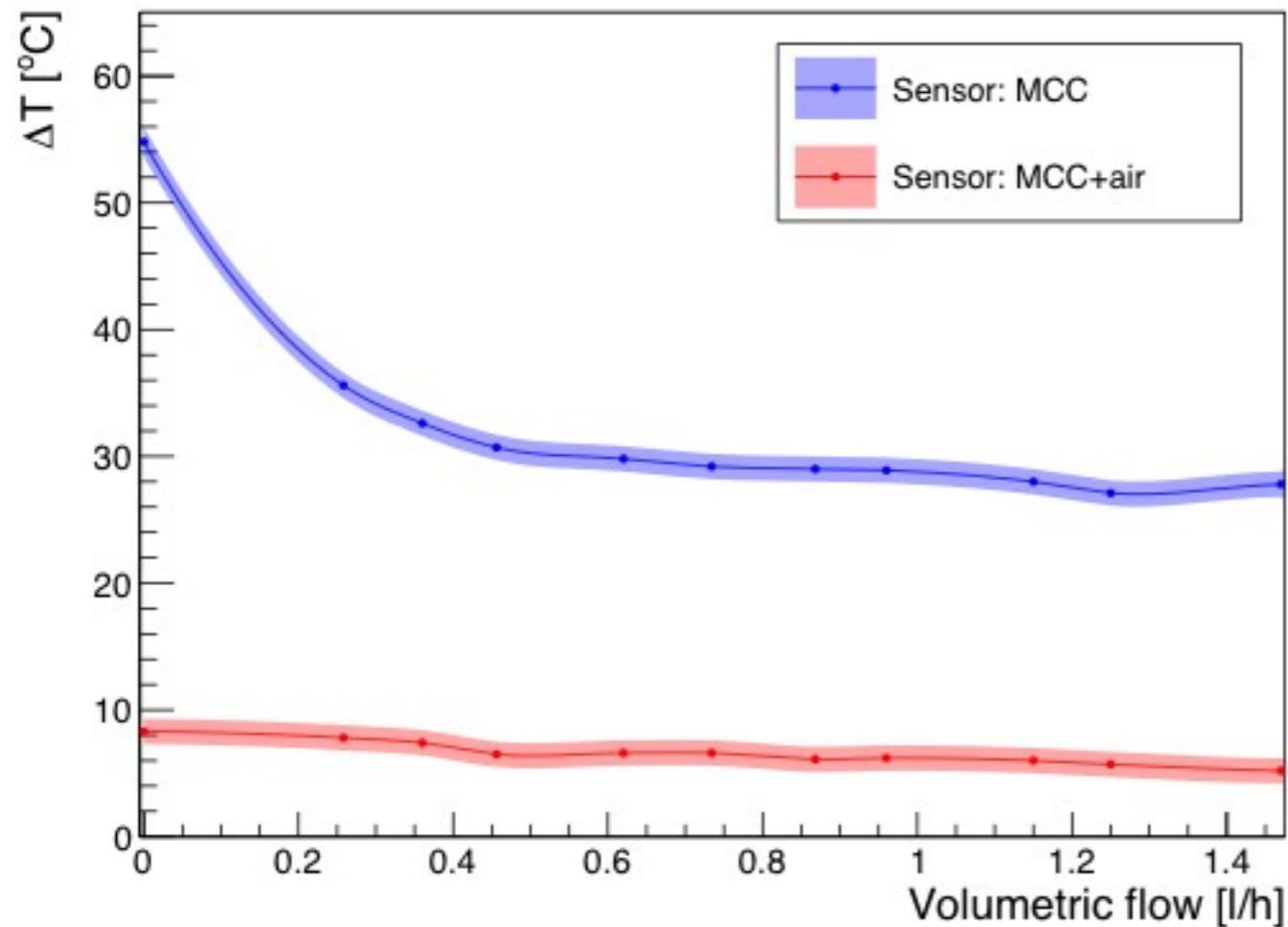


Cooling strategy: micro-channels running under the front end and gentle air flow on the sensor part

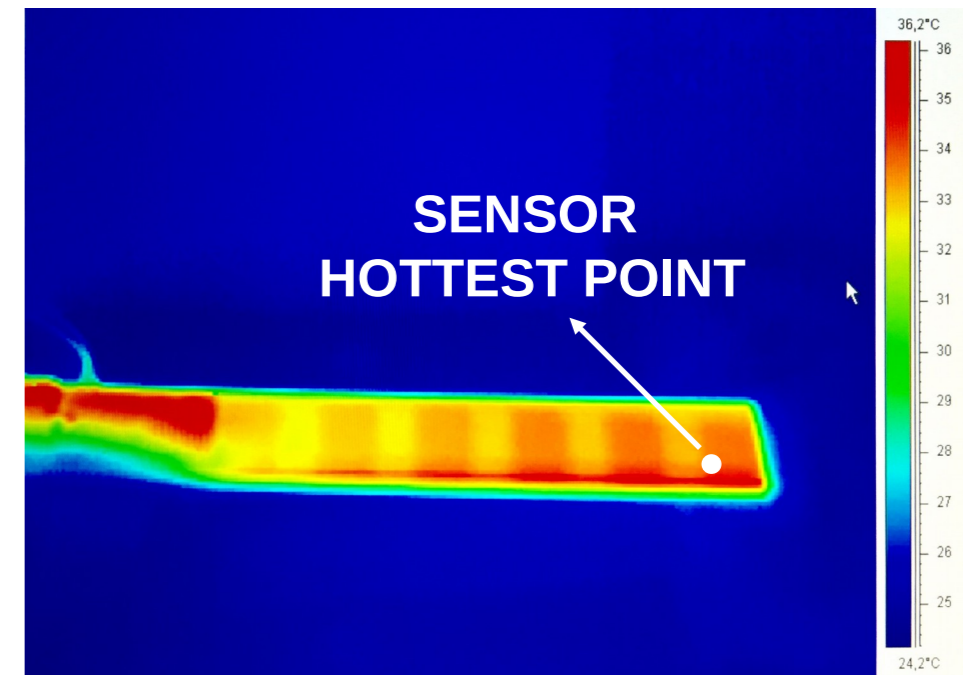


- There is not big difference between MCC and MCC+air at the DCD hottest point
- Farthest regions to the air inlet are less affected
- Even with low volumetric water flow, high cooling
- 93% of total heat removed by MCC

Thermal measurements: MCC + air

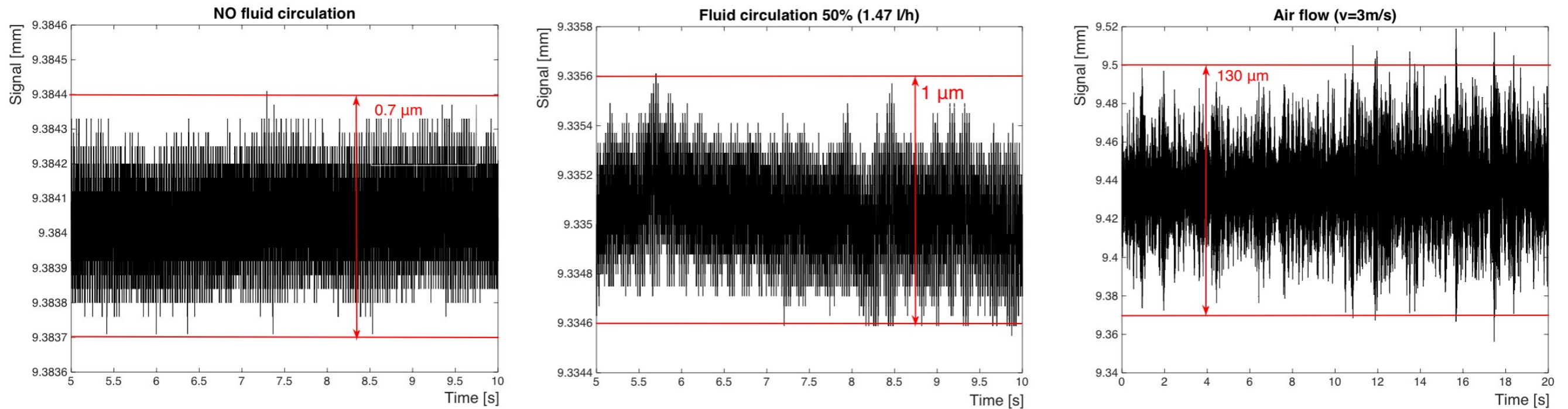


Cooling strategy: micro-channels running under the front end and gentle air flow on the sensor part



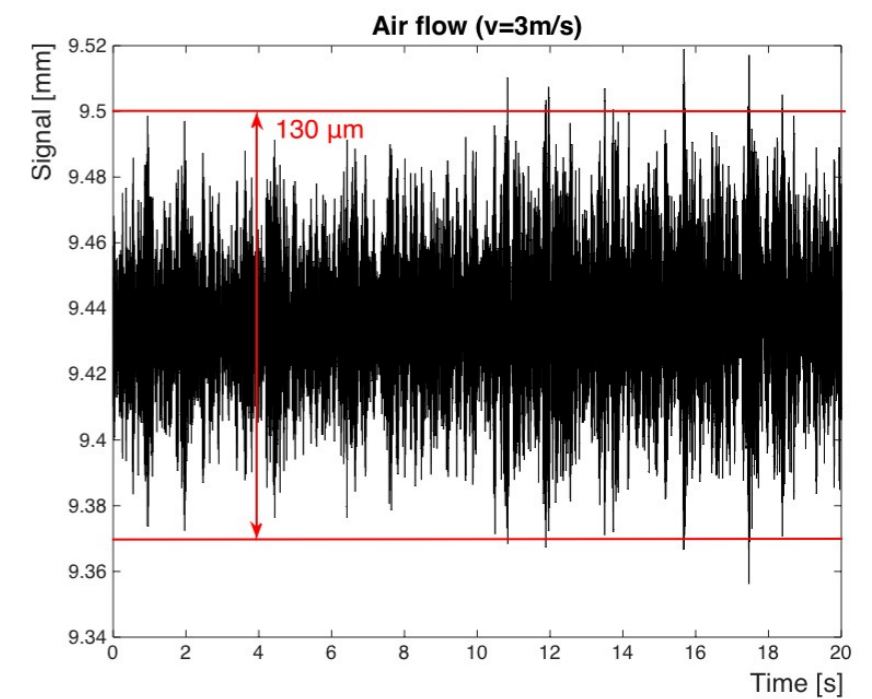
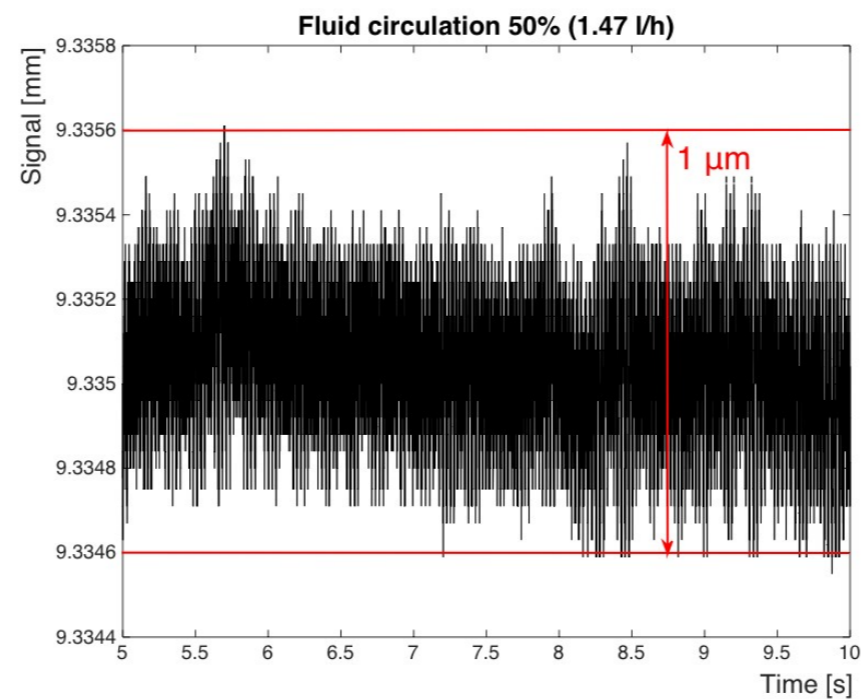
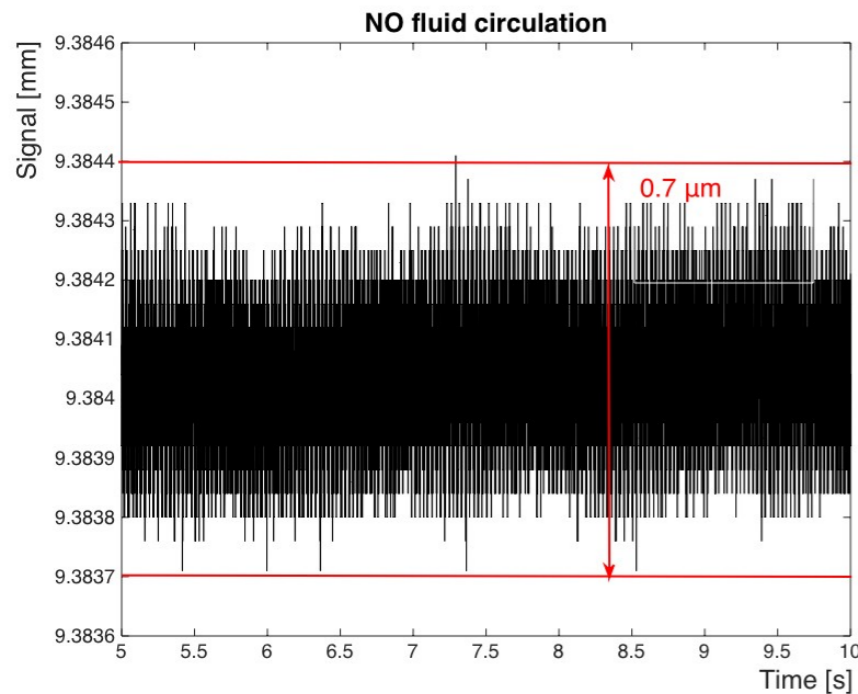
- Big difference between MCC and MCC+air at the sensor area hottest point
- Nearest regions to air input are efficiently cooled even with low air flow
- MCC has less impact in away points as expected and great cooling locally

Vibrations and deformations



Clamped-free (CF) configuration: One extreme of the dummy is clamped to the 3D adaptor while the other is free of movement

Vibrations and deformations



**No fluid circulation
and no air flowing**

Peak to peak of the
signal $\sim 0,7 \mu\text{m}$
RMS $\sim 0,3 \mu\text{m}$

**Fluid circulation
1,47 l/h**

Peak to peak of the
signal $\sim 0,1 \mu\text{m}$
RMS $\sim 0,4 \mu\text{m}$

**Air flowing
3 m/s**

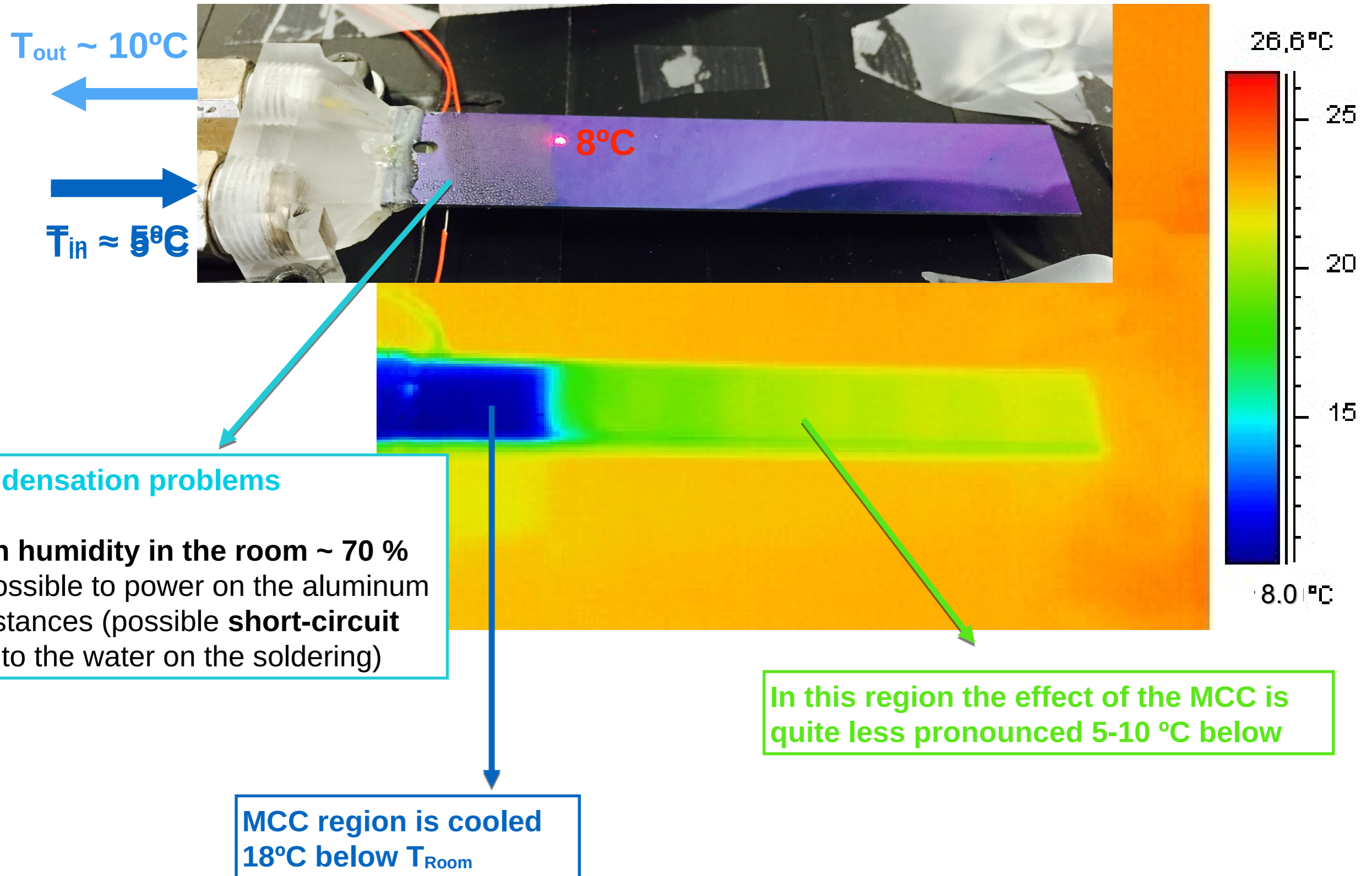
Peak to peak of the
signal $\sim 130 \mu\text{m}$
RMS $\sim 57 \mu\text{m}$

MCC has no significant impact on mechanical stability in the clamped-free configuration but air deformations are more than 100 μm if $v=3\text{m/s}$ (could be reduced a factor 10 for velocities under $\leq 0.5\text{m/s}$)

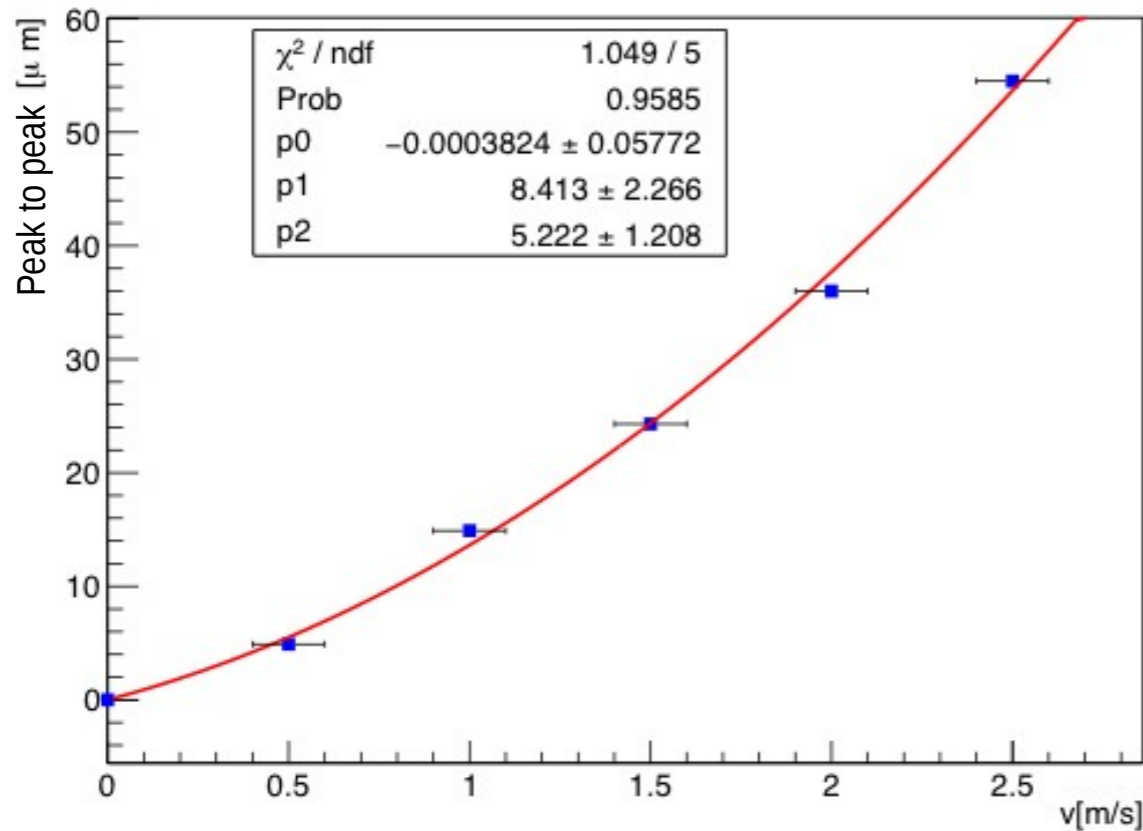
Pressure test



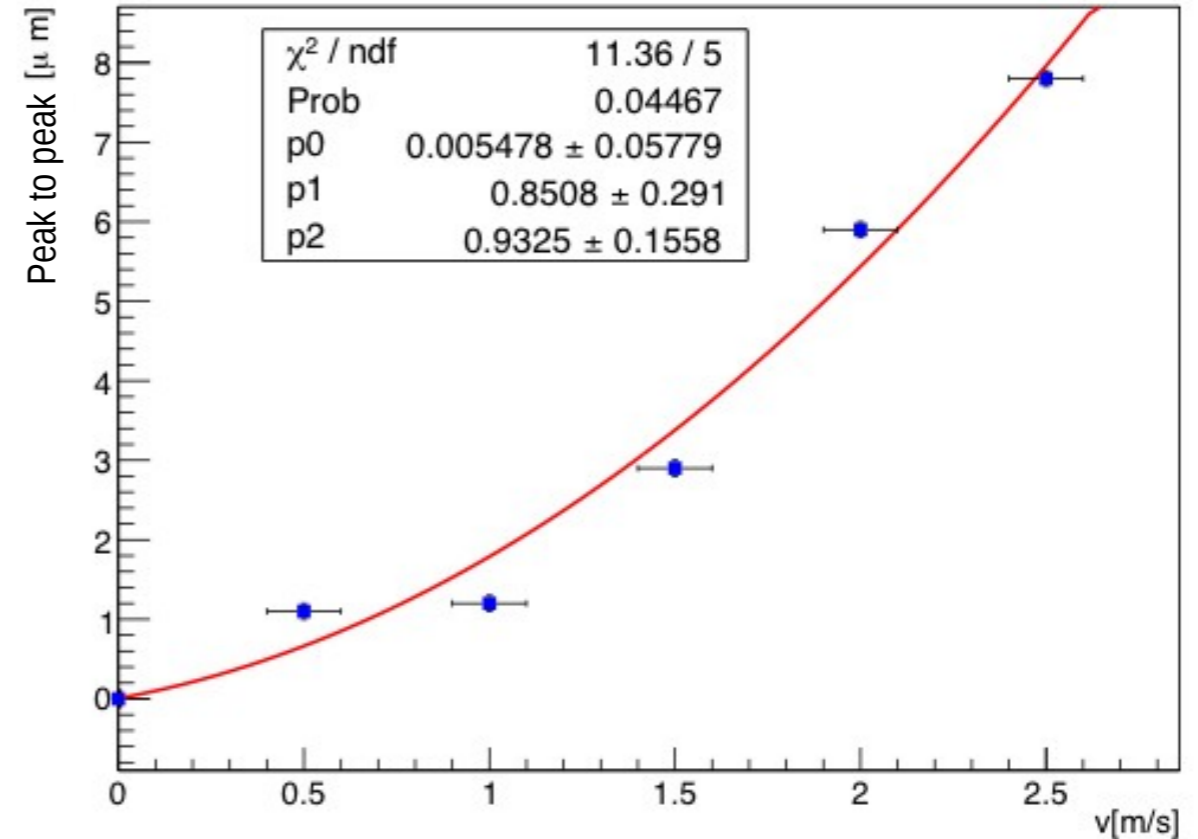
Thermal measurements: cold water



Amplitude vs v_{air}



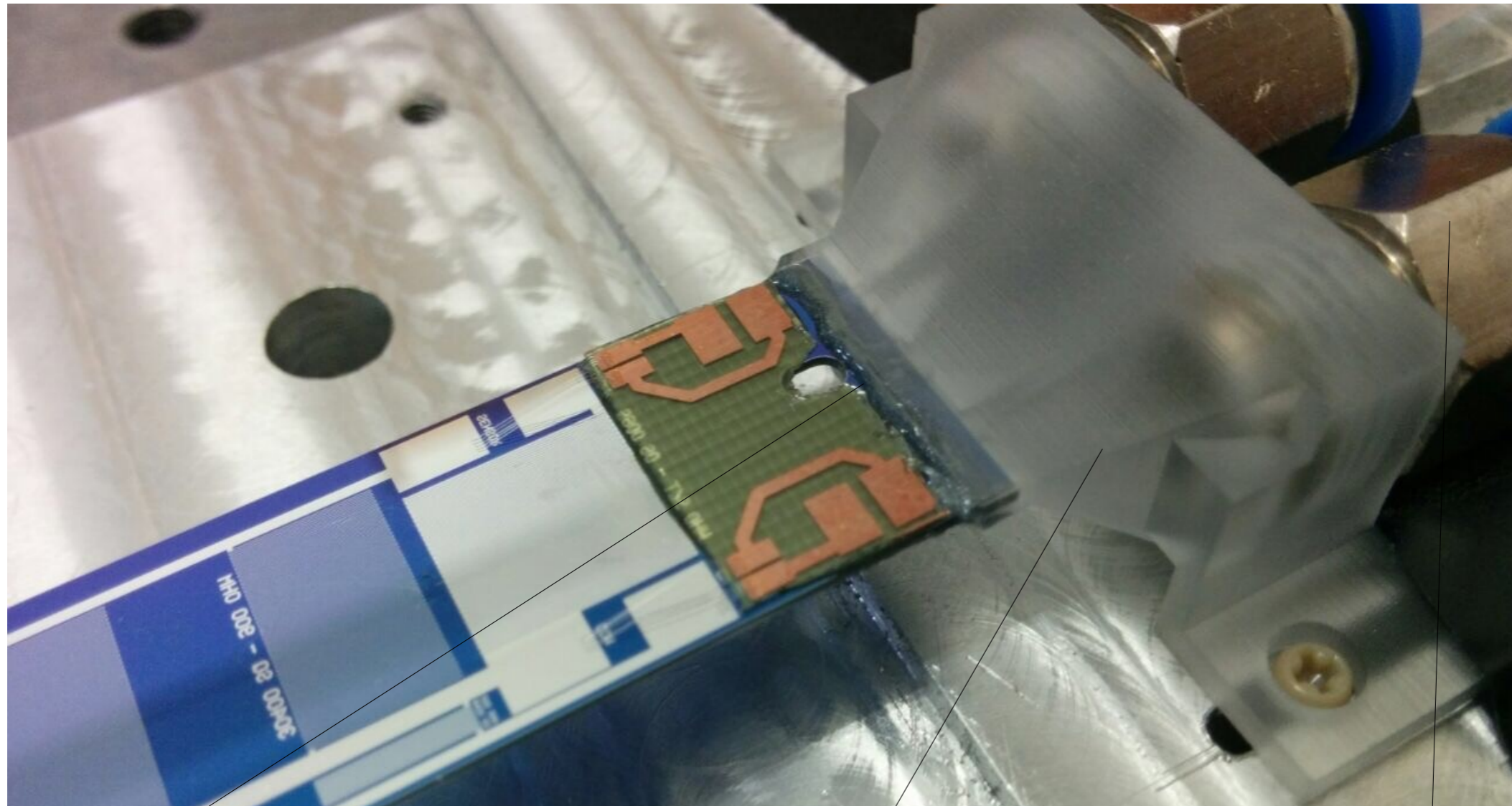
Clamped-Free



Clamped-Clamped

- Peak-to-peak amplitude is the change between peak (highest amplitude value) and *trough* (lowest amplitude value)
- $\text{RMS} \simeq (\text{PeaktoPeak}/2) * 0.707$ (approximation)
- For $v = 2.5 \text{ m/s}$ the amplitude of vibration is:
 - **$\sim 19 \mu\text{m}$** for **clamped-free** configuration
 - **$\sim 2.8 \mu\text{m}$** for **clamped-clamped** configuration

3D-printed adaptor PREVIOUS design: problems



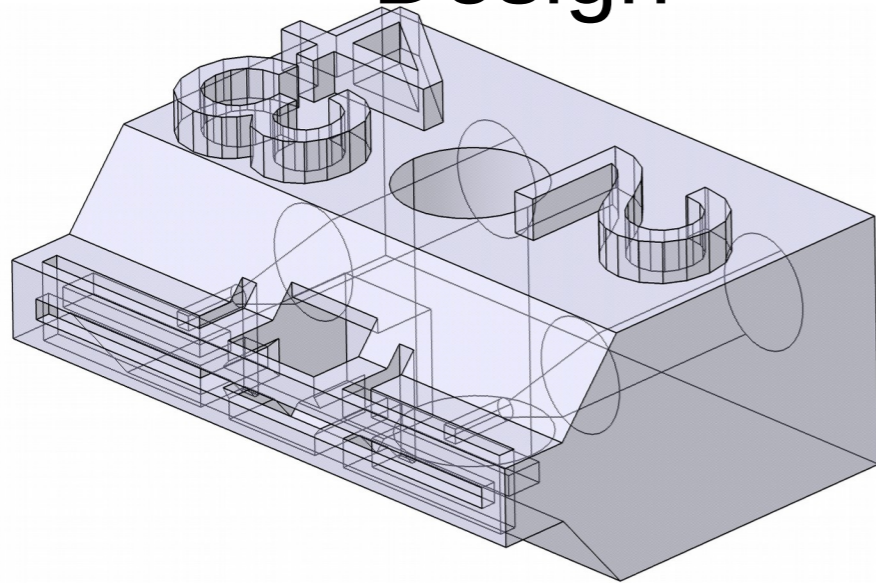
Glue: leaks

3D printed part:
massive $\rightarrow X/X_0=0,81\%$

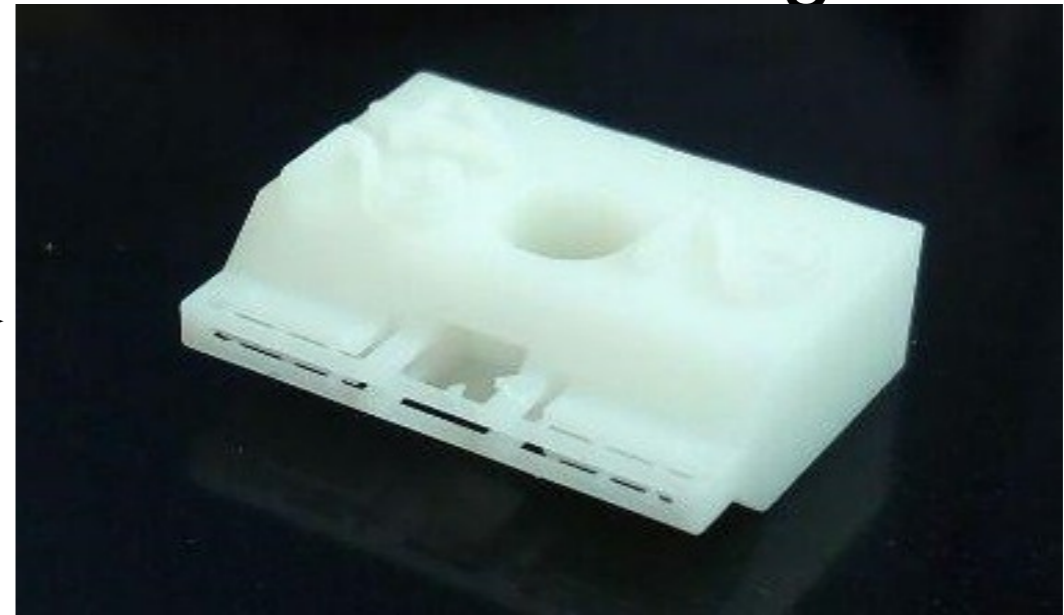
Connectors: space
and massive

3D-printed adaptor CURRENT design

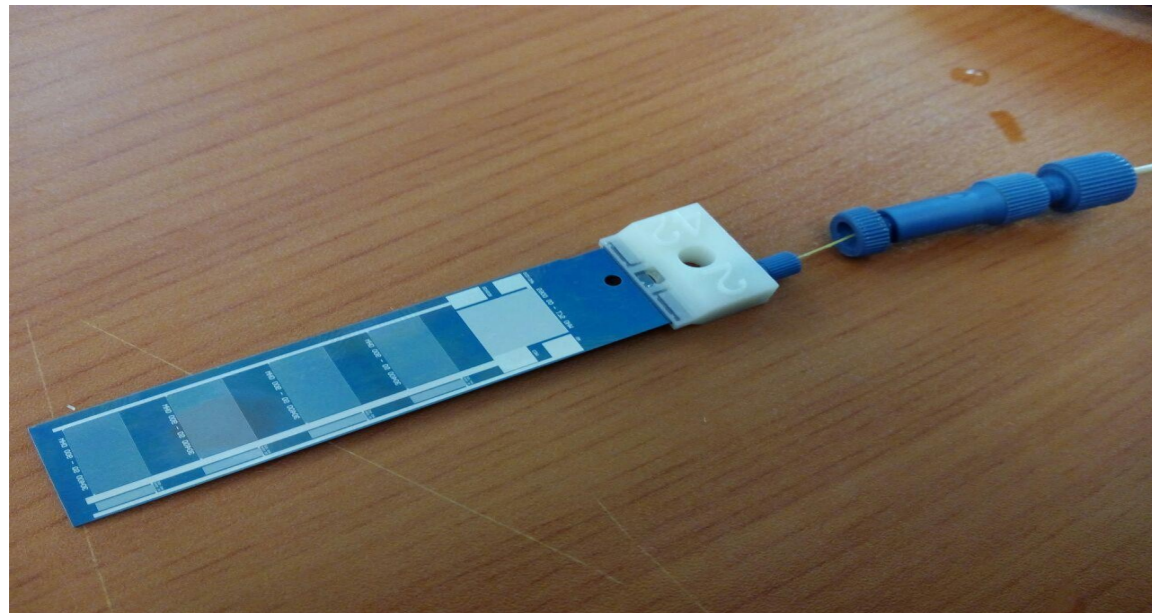
Design



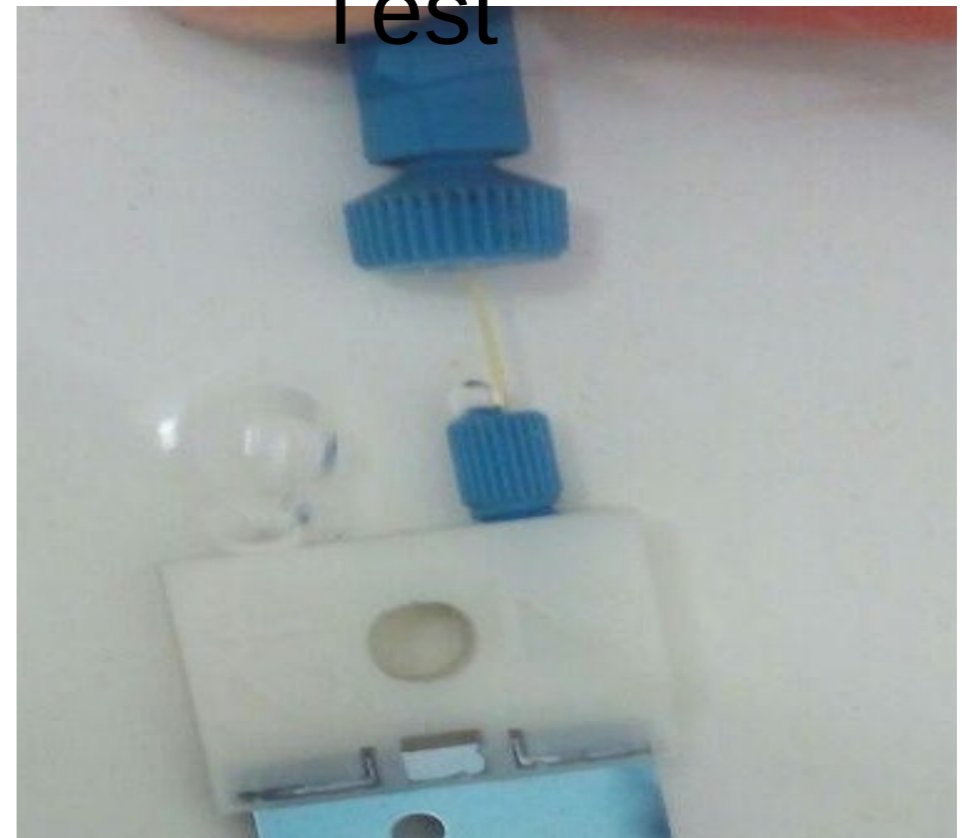
3D-Printing



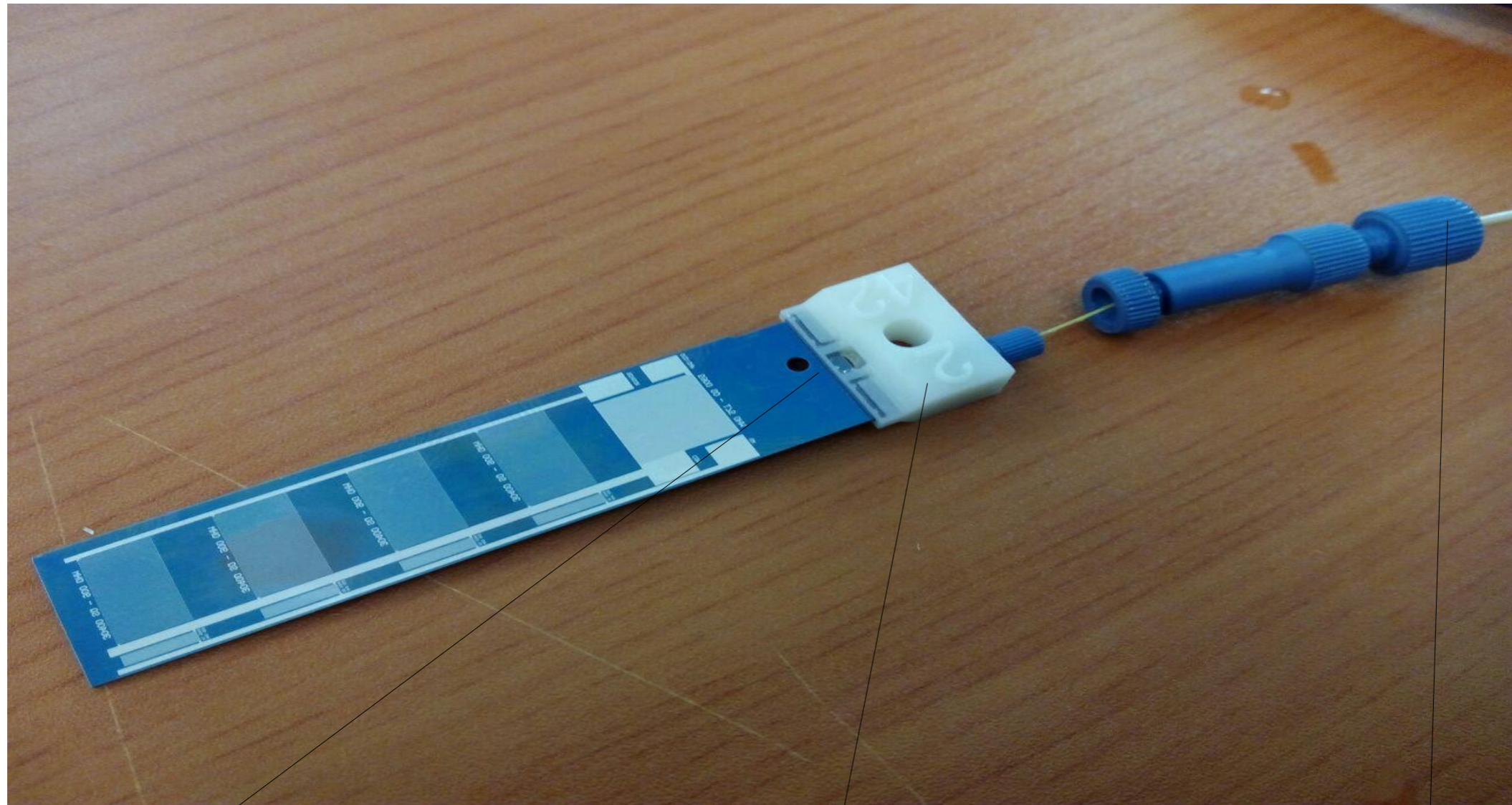
Gluing



Test



3D-printed adaptor CURRENT design: Characteristics

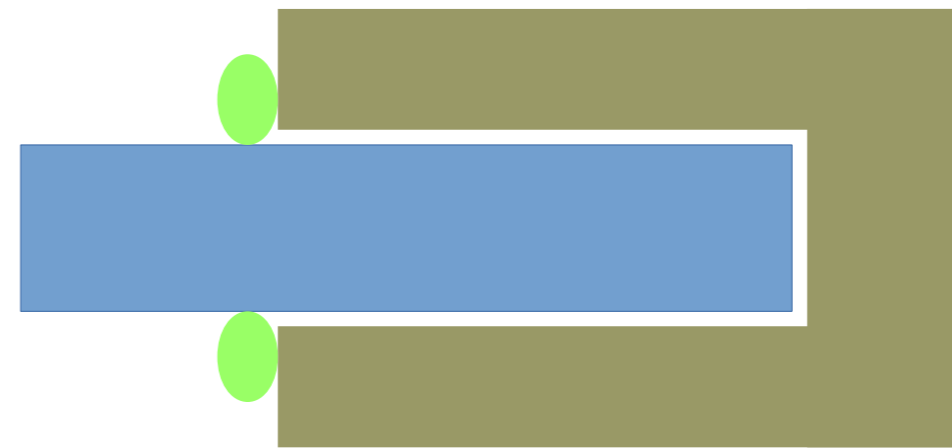


Glue:
Araldite2020

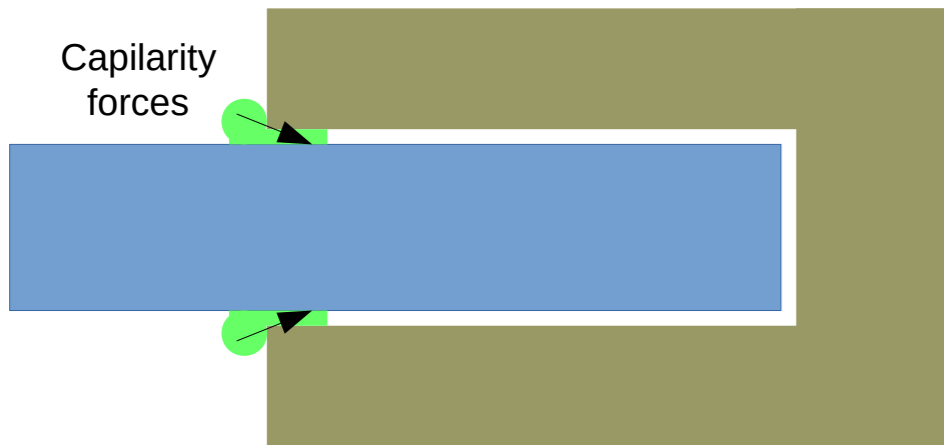
3D printed part: less
massive $\rightarrow X/X_0=0,21\%$

Connectors: far
from VX region

3D-printed adaptor CURRENT design: Glue issue



Capilarity
forces



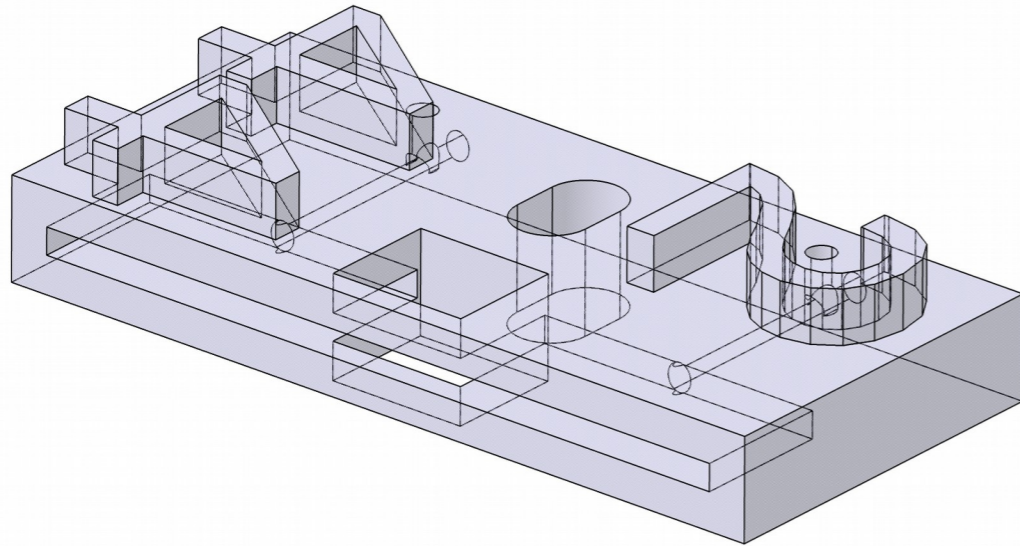
Glue:
Araldite2020

Expected max.
pressure: 150bar

Possible problem:
Clog of MC

3D-printed adaptor FUTURE design

Design



3D-Printing

$$X/X_0=0,05\%$$

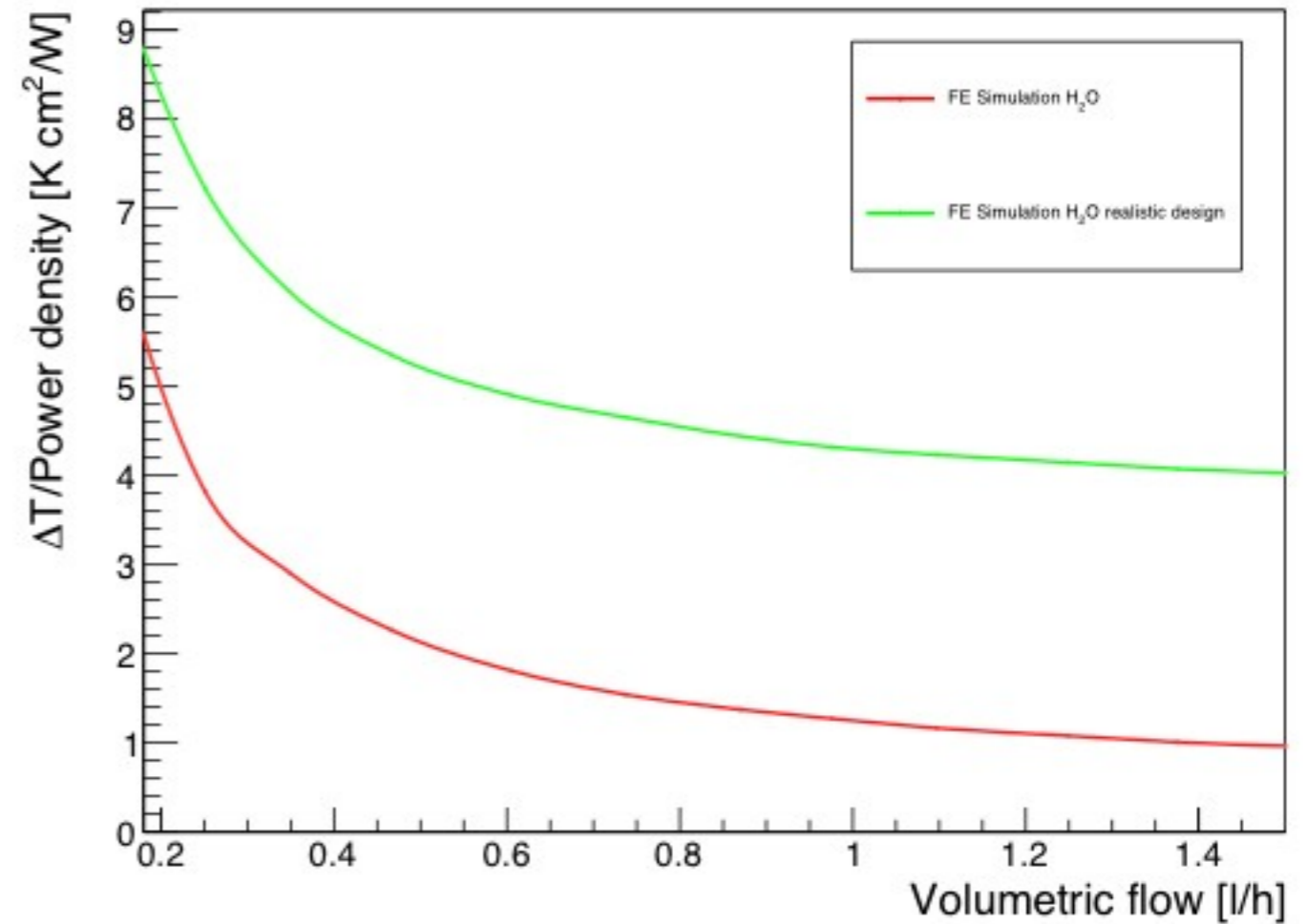
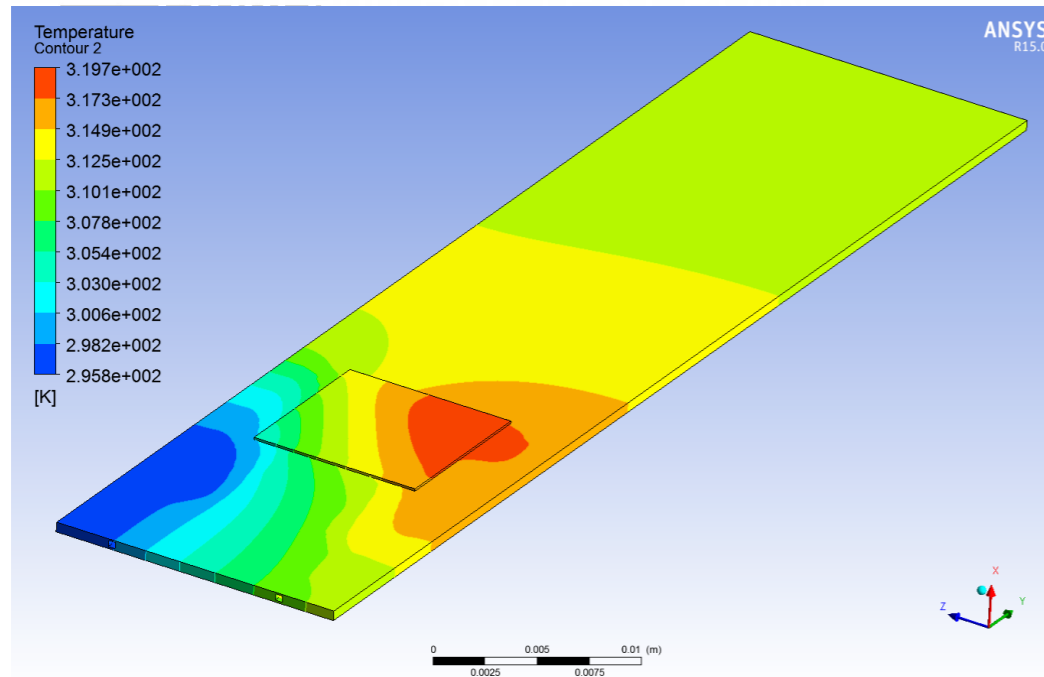
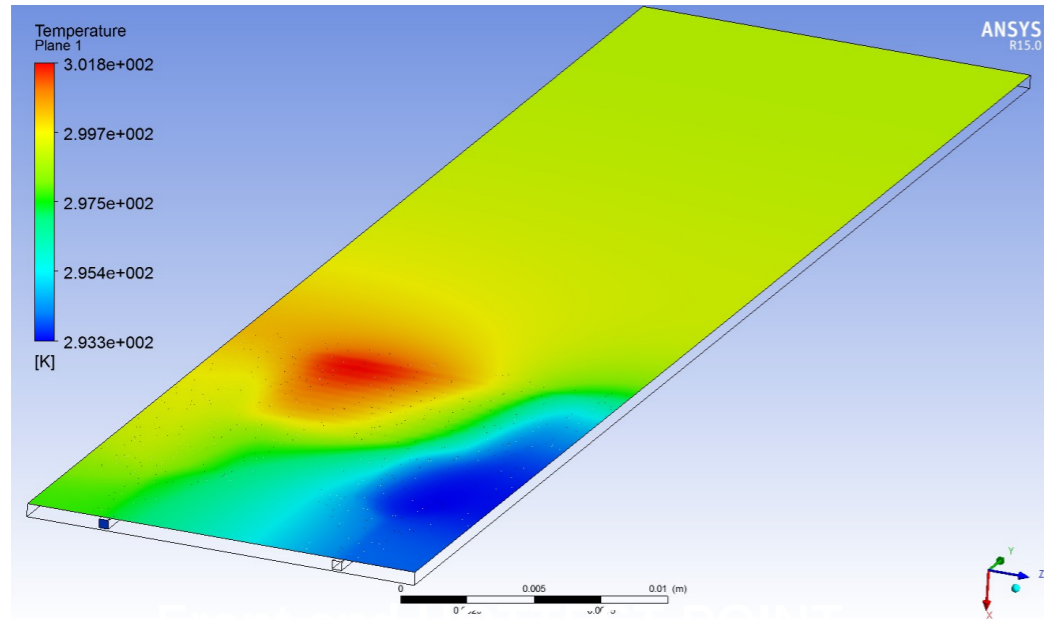
Gluing

To try different types of glue:
2020
2011
Epolite

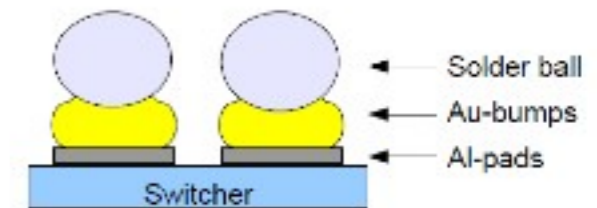
Test

Possibility to include:
1) Bumpbondings (next slides)
2) Thermoresistors (next slides)
3) New MC layout (next slides)
4) Automatize gluing process

Thermal simulations: bumpboundings



Realistic design
300 μm Si ASICS +
100 μm Bump-boundings
thermal resistivity of 6 W/m·K

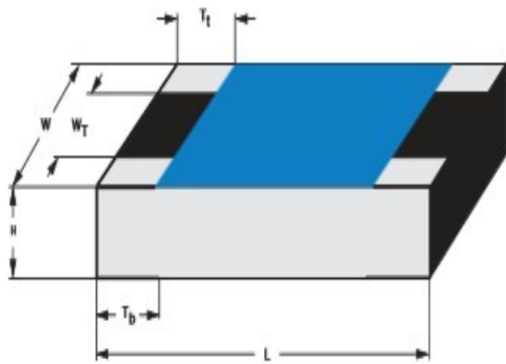


C.Mariñas PhD thesis

<http://digital.csic.es/bitstream/10261/41942/1/Carlos%20Mari%C3%B1as-Tesis.pdf>

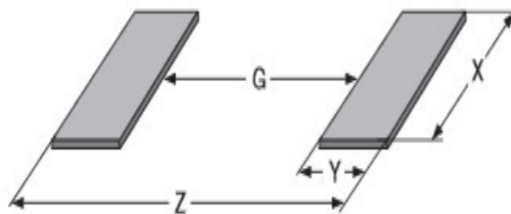
In the realistic design the power dissipation is degraded

Thermal simulations: bumpbondings

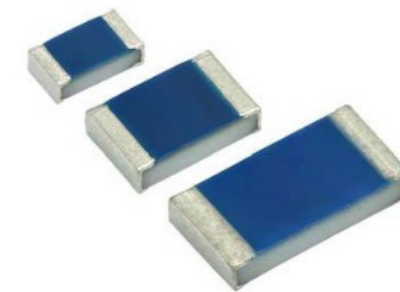


DIMENSIONS - PTS sensor types, mass and relevant physical dimensions							
TYPE	H	L	W	W _T	T _t	T _b	MASS (mg)
PTS 0603	0.45 + 0.1/- 0.05	1.55 ± 0.05	0.85 ± 0.1	> 75 % of W	0.3 + 0.15/- 0.2	0.3 + 0.15/- 0.2	1.9
PTS 0805	0.45 + 0.1/- 0.05	2.0 ± 0.1	1.25 ± 0.15	> 75 % of W	0.4 + 0.1/- 0.2	0.4 + 0.1/- 0.2	4.6
PTS 1206	0.55 ± 0.1	3.1 + 0.1/- 0.2	1.6 ± 0.15	> 75 % of W	0.5 ± 0.25	0.5 ± 0.25	9.2

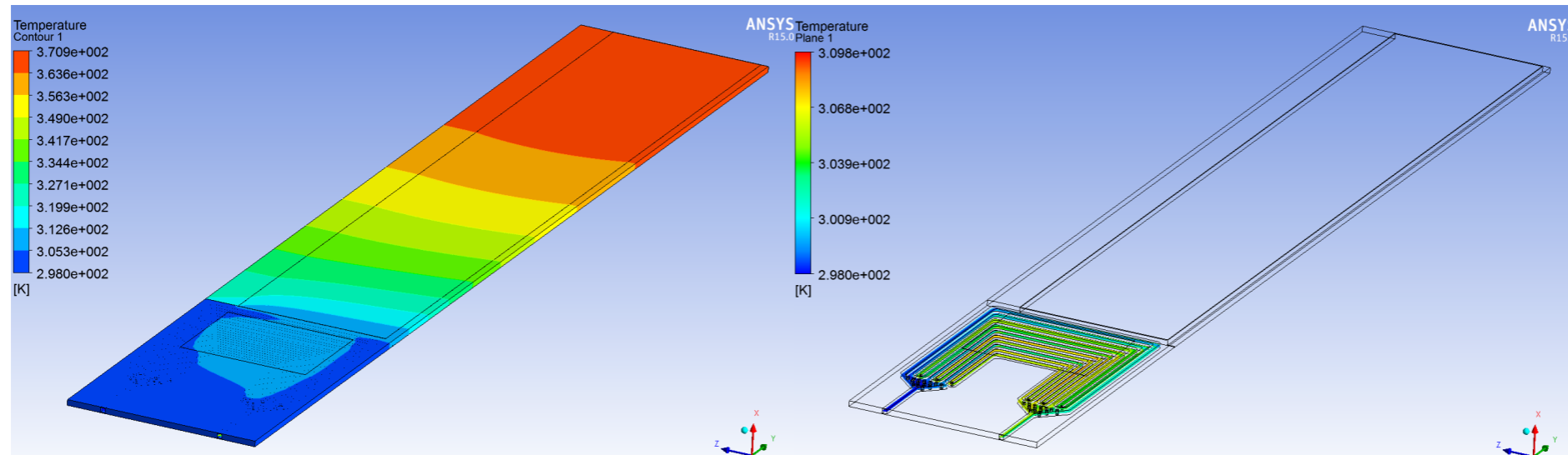
SOLDER PAD DIMENSIONS in millimeters



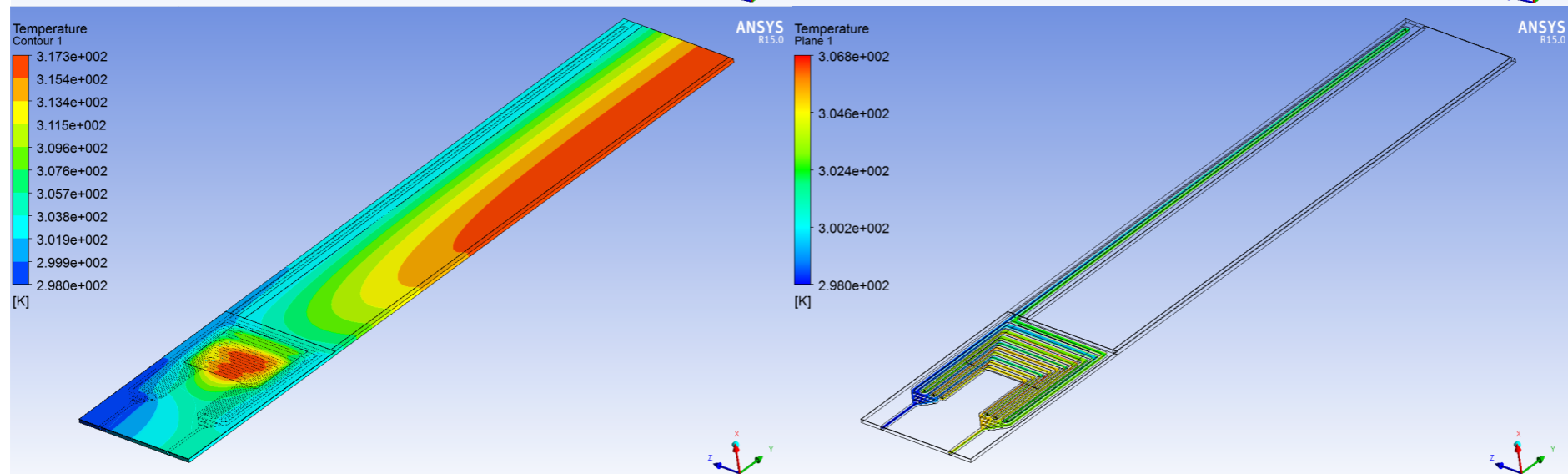
RECOMMENDED SOLDERPAD DIMENSIONS								
TYPE	WAVE SOLDERING				REFLOW SOLDERING			
	G	Y	X	Z	G	Y	X	Z
PTS 0603	0.55	1.1	1.1	2.75	0.65	0.7	0.95	2.05
PTS 0805	0.8	1.25	1.50	3.2	0.9	0.9	1.4	2.7
PTS 1206	1.4	1.5	1.9	4.4	1.5	1.15	1.75	3.8



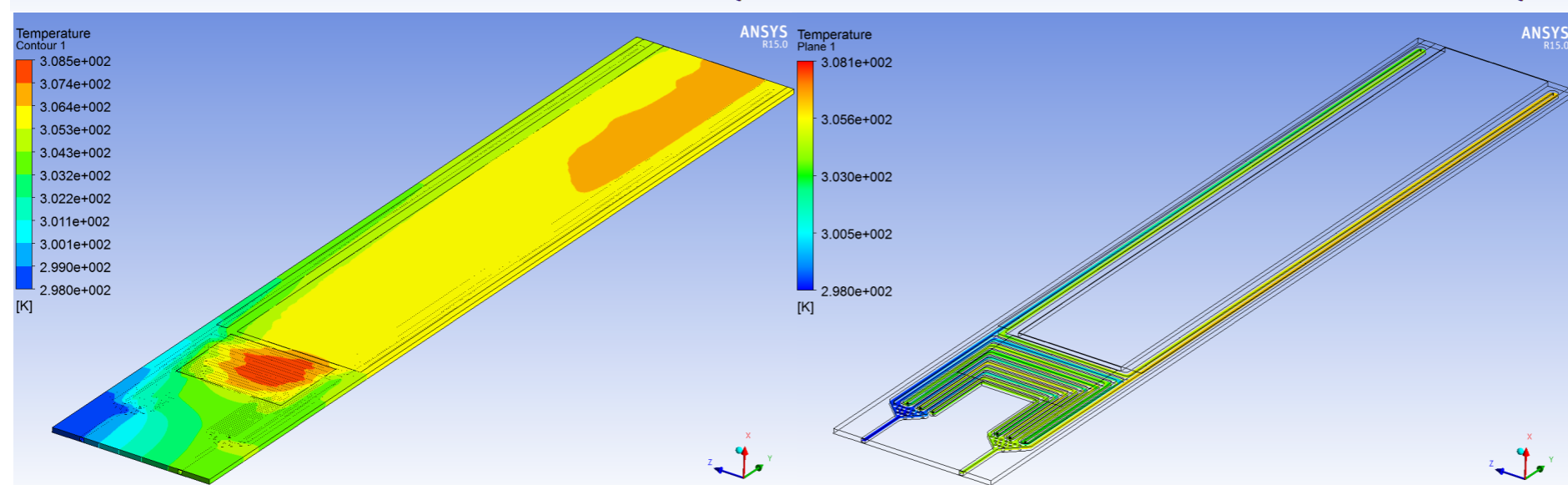
Thermal simulations: Layouts



**Standard
MCC layout**
 $\Delta T = 73 \text{ K}$



**Standard
MCC layout +
channel below
switchers**
 $\Delta T = 15 \text{ K}$



**Standard
MCC layout +
channel below
switchers +
channel in the
balcony**
 $\Delta T = 5 \text{ K}$